



SECTION II

Working in a Reduced Gravity Environment: “A Primer”

Kenol Jules

PIMS Project Scientist

NASA Glenn Research Center

March 6th, 2001



REDUCED GRAVITY ENVIRONMENT DESCRIPTION

The reduced gravity acceleration environment of an orbiting spacecraft in a low earth orbit is a very complex phenomenon. Many factors contribute to form the overall environment. In general, it can be considered as made up of the following three components:

QUASI-STEADY: is composed of those accelerations that vary over long periods of time, typically longer than a minute for space-based platforms.

VIBRATORY: is composed of those accelerations that are harmonic and periodic in nature with a characteristic frequency.

TRANSIENT: is composed of those accelerations that last for a short period time, and are non-repetitive.

REDUCED GRAVITY ENVIRONMENT DESCRIPTION

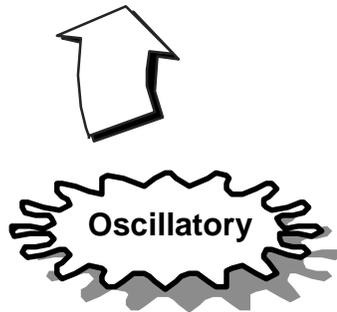
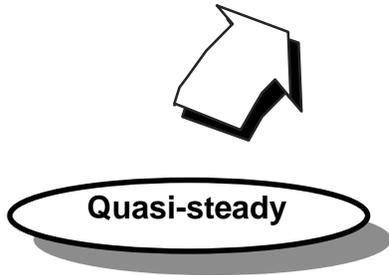
What is a "reduced gravity environment" ?



Major properties

Reduced gravity environment

An environment in which the effects of gravity are small compared to those effects we experience on earth



REDUCED GRAVITY ENVIRONMENT DESCRIPTION

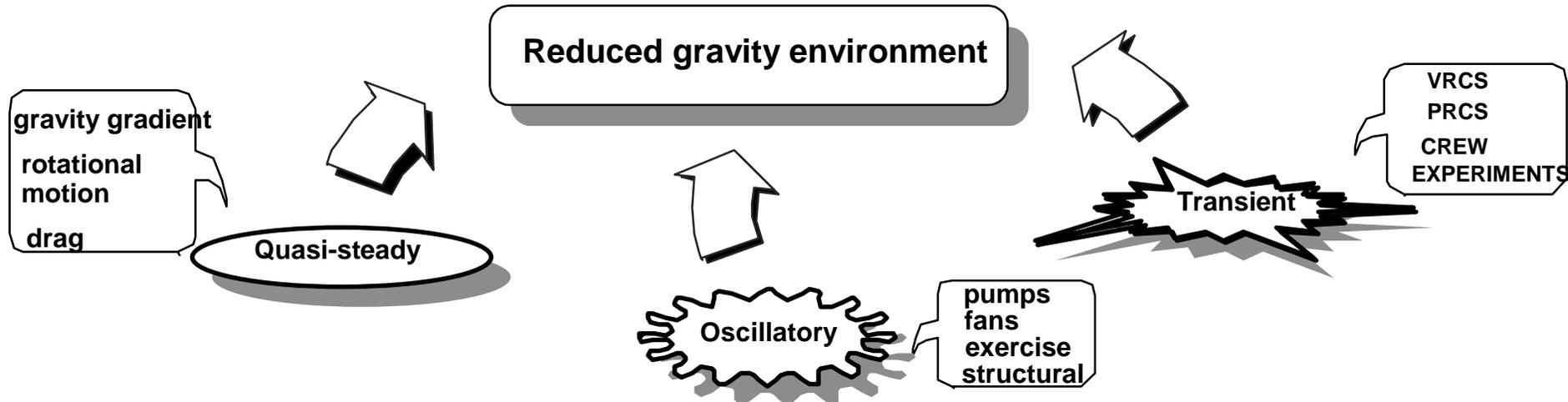
What is a "reduced gravity environment" ?



Major properties



What causes these accelerations?



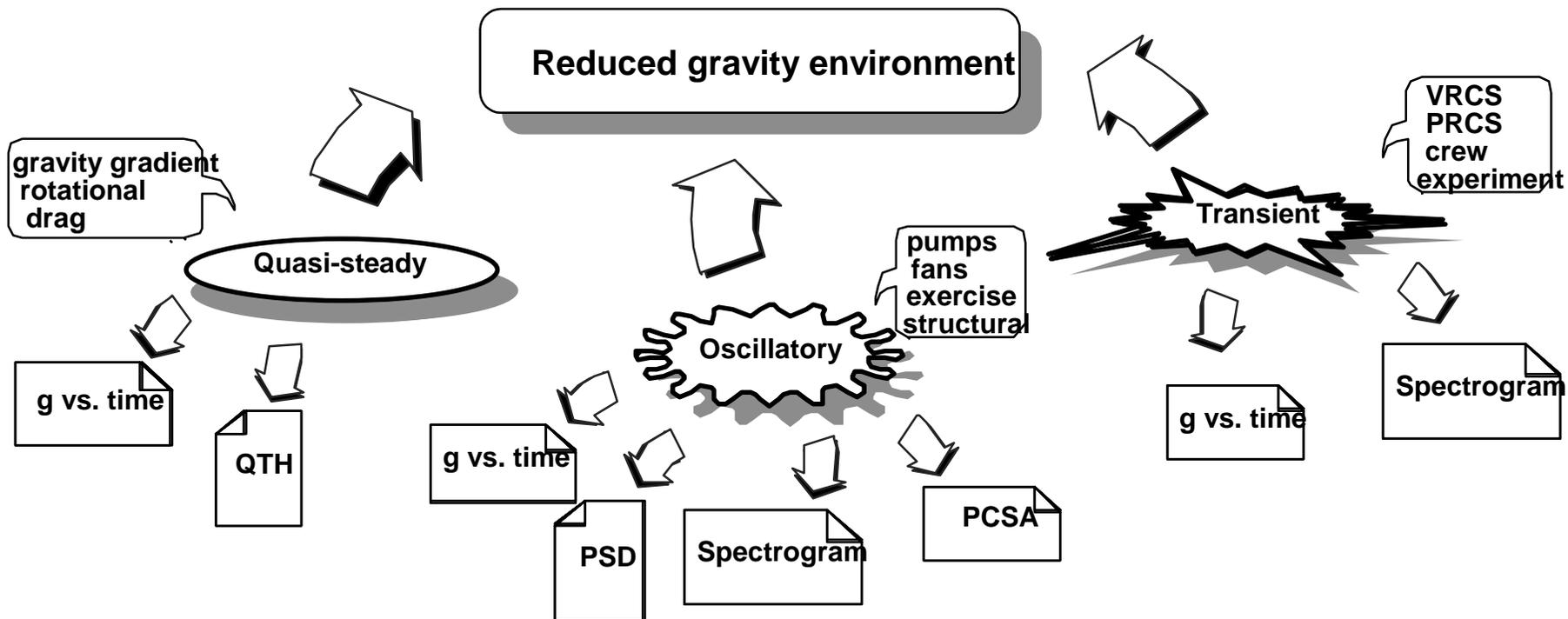
REDUCED GRAVITY ENVIRONMENT DESCRIPTION

What is a "reduced gravity environment" ?

Major properties

What causes these accelerations

How do we display them?

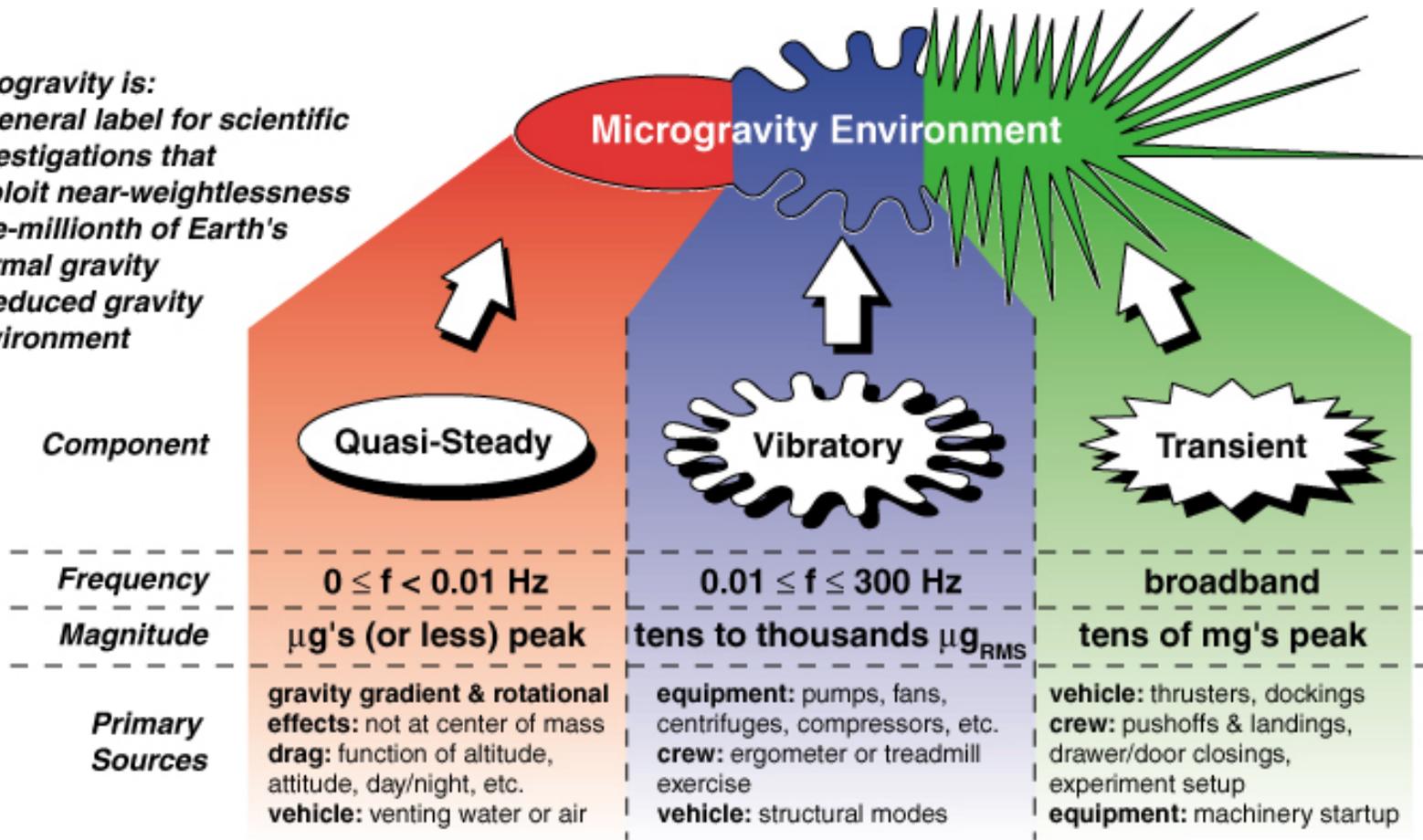


REDUCED GRAVITY ENVIRONMENT DESCRIPTION

Components of the Reduced Gravity Environment

Microgravity is:

- a general label for scientific investigations that exploit near-weightlessness
- one-millionth of Earth's normal gravity
- a reduced gravity environment





REDUCED GRAVITY ENVIRONMENT DESCRIPTION

WHAT DO ALL THESE MEAN TO YOU?

- The environment is **NOT** “zero-g”!
- Experiments may be affected by the reduced gravity environment
- This tutorial will explain to you what the environment is likely to be, how we measure it, how we interpret it, and will show you what impact the environment has had on some experiments.



Working in a Reduced Gravity Environment : “A Primer”



REDUCED GRAVITY ENVIRONMENT DESCRIPTION

Reduced gravity Facilities	Duration	Acceleration Levels	Notes
Drop Towers	< 10 seconds	10^{-3} g	NASA, Japan, Germany
Parabolic Aircraft	15 – 25 seconds	1.5×10^{-2} g	~ 40 parabolas per campaign
Rockets	Up to 600 seconds	10^{-5} g	Various countries
SPACEHAB Module	Up to 16 days	$< 5.5 \times 10^{-4}$ g (for the combined three axes)	Frequency range: 0.01 – 25 Hz
Spacelab Module (MPSS)	Up to 16 days	$< 1.4 \times 10^{-3}$ g (for the combined three axes)	Frequency range: 0.01 – 25 Hz
Spacelab Module	Up to 16 days	$< 3 \times 10^{-3}$ g (for the combined three axes)	Frequency range: 0.01 – 25 Hz
STS overall Quasi-Steady environment	Up to 15 days	$< 1 \times 10^{-6}$ g	Frequency range: 0.0 – 0.01 Hz. Average values for typical orbiter attitudes
STS overall vibratory environment	Up to 15 days	Tens to thousands μg_{RMS}	Depending on what activity is taking place
STS overall transient environment	Up to 15 days	Tens of μg peak	Depending on what activity is taking place

NOTE:

The acceleration level values listed in this table are NOT to be used as a nominal value of the reduced gravity environment of any specific platform. The environment is very dynamic in nature. They are listed here to illustrate the non-zero nature of the reduced gravity environment. The actual value for any of the platform listed here, at any moment in time, is frequency dependent (mission timeline activity dependent).



SOME DEFINITIONS

Acceleration Measurement Systems

- **OARE:** Orbital Acceleration Research Experiment - instrument which measures low frequency accelerations from DC up to 0.01 Hz
- **MAMS:** Microgravity Acceleration Measurement System - instrument which measures acceleration levels to characterize the ISS reduced gravity environment provided to users. MAMS measures accelerations from DC to 1 Hz.
- **SAMS:** Space Acceleration Measurement System - instrument which measures accelerations from 0.01 Hz to 100 Hz on Shuttle, Mir, and KC-135.
- **SAMS-II:** Second generation SAMS - instrument which will measure accelerations from 0.01 Hz to 300 Hz on the ISS.
- **SAMS-FF:** SAMS for Free Flyers - instrument for free flyers (e.g. sounding rockets), Shuttle, and KC-135 which measures linear and roll-rate accelerations. Measure accelerations from 0.01 to 300 Hz.



SOME DEFINITIONS

- **reduced gravity environment:** an environment in which the effects of gravity are small compared to those we experience on Earth
- **oscillatory:** term used to describe vibratory disturbances with frequency content greater than 0.01 Hz
- **transient:** signals that are impulsive in nature; passing quickly into and out of existence
- **quasi-steady:** a signal which varies at a very low frequency, typically below 0.01 Hz

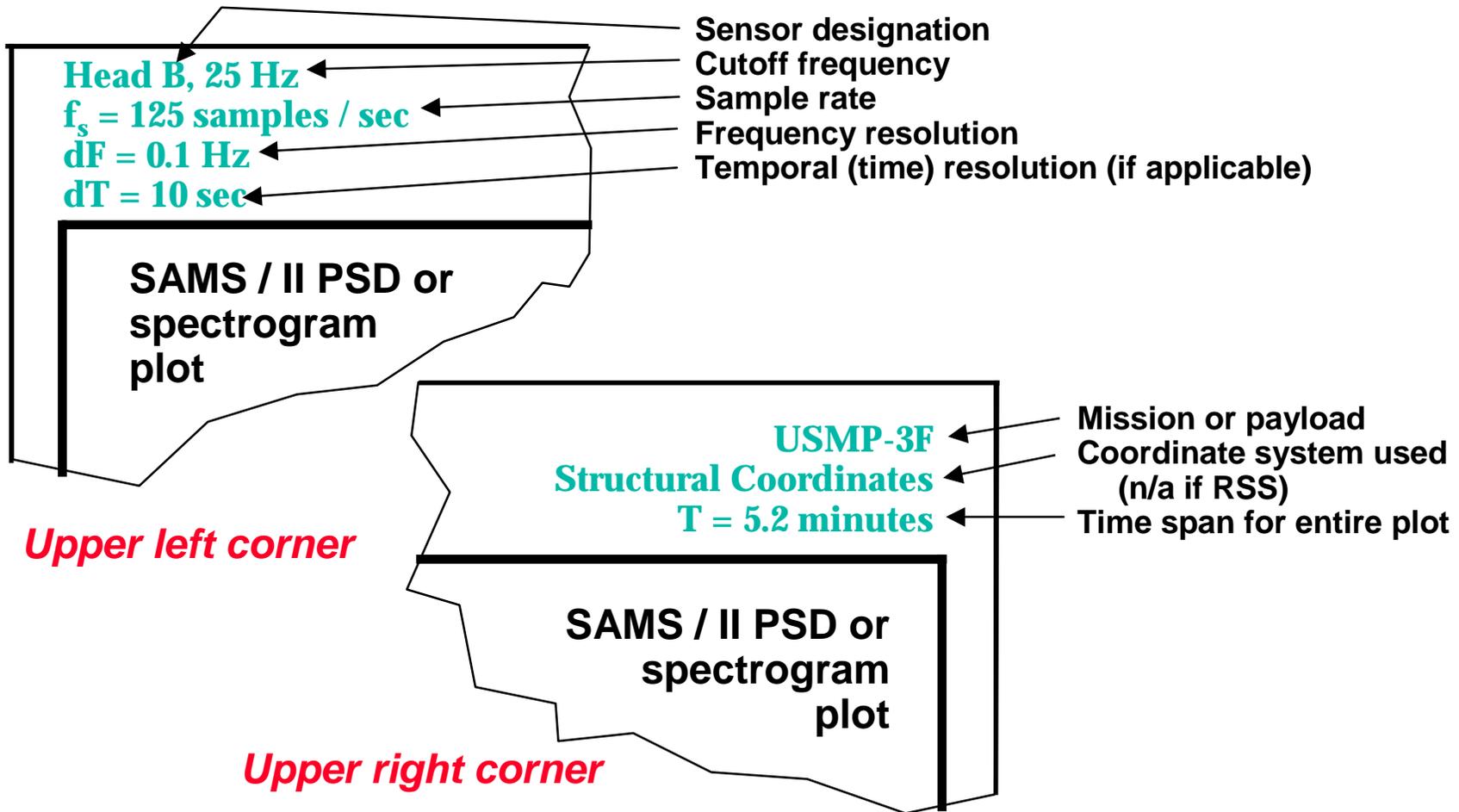


SOME DEFINITIONS

- **Nyquist criteria:** sampling rate must be at least twice that of the highest frequency contained in the signal of interest
- **cutoff frequency (f_c):** corner frequency in filter response; highest unfiltered frequency of interest
- **sample rate (f_s):** rate at which an analog signal is sampled ($\text{samples}/\text{sec}$)
- **power spectral density:** a function that quantifies the distribution of power in a signal with respect to frequency
- **spectrogram:** a 3-D representation of the power spectral density as a function of frequency and time

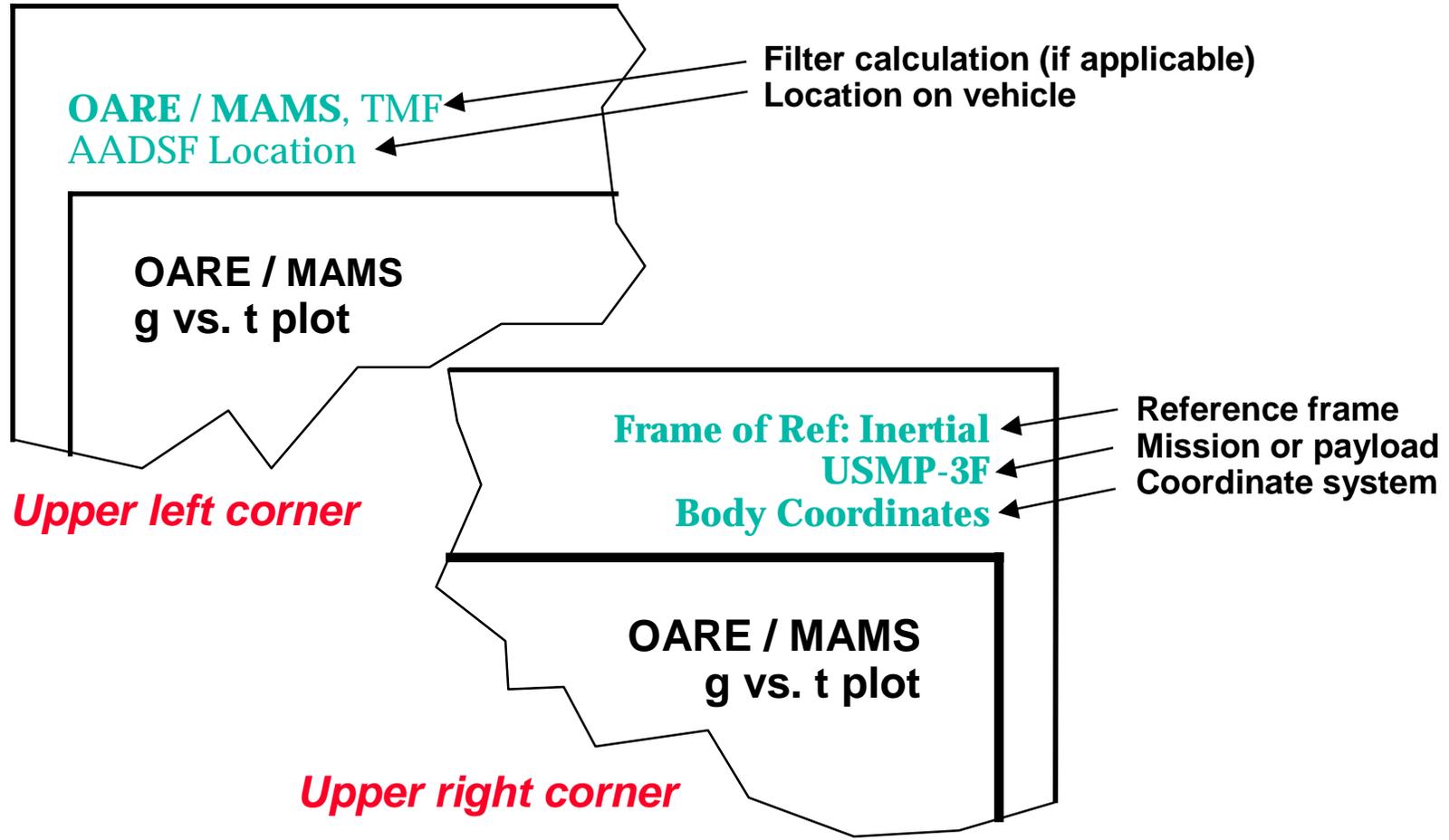
SAMPLE PLOTS INFORMATION

SAMS / II



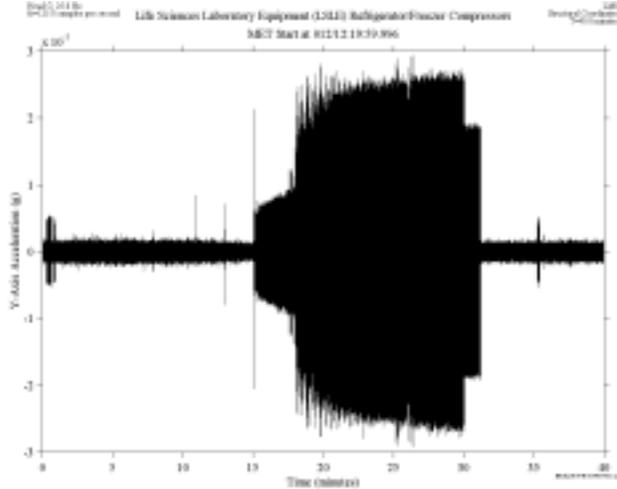
SAMPLE PLOTS INFORMATION

OARE / MAMS

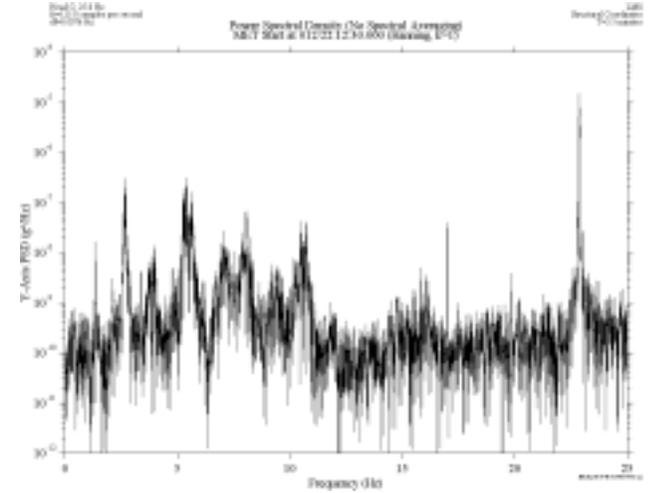


SOME PLOT SAMPLES

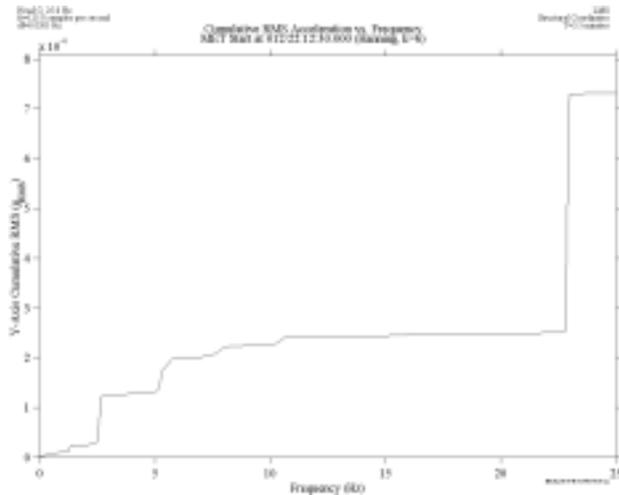
Acceleration vs. Time



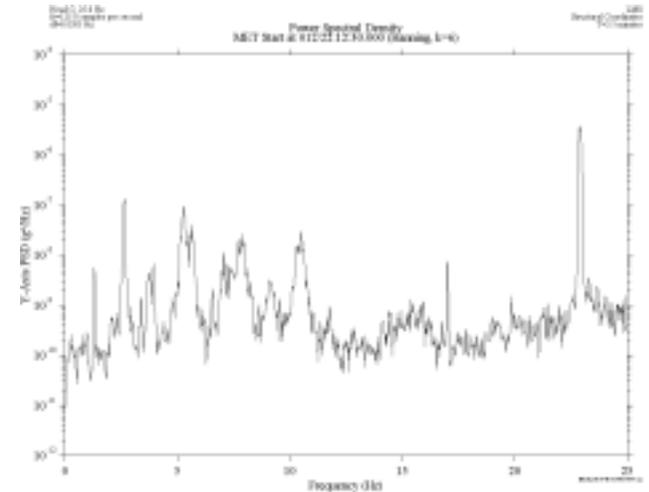
Power Spectral Density –no spectral averaging



Cumulative RMS acceleration vs. Frequency

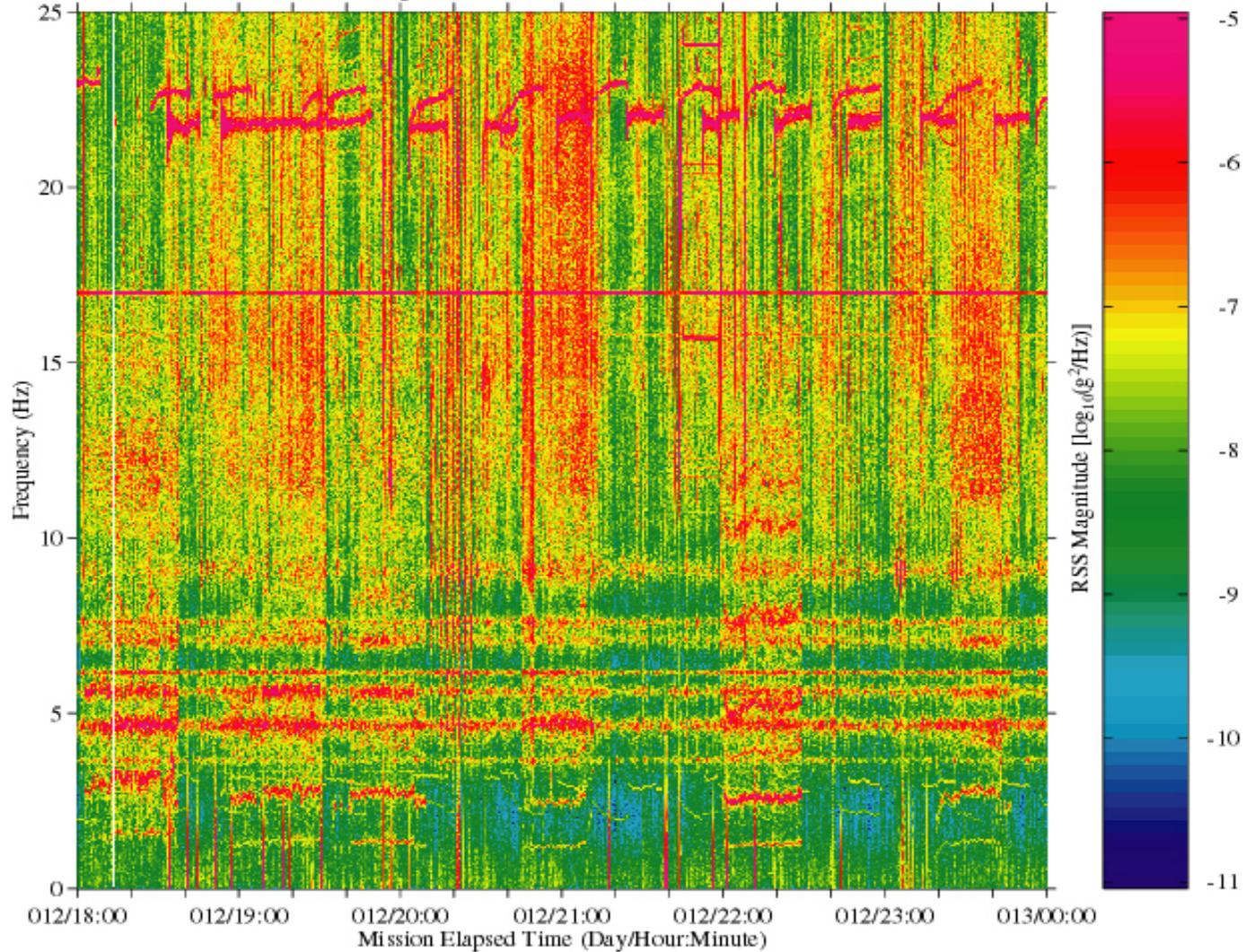


Power Spectral Density – with averaging



SOME PLOT SAMPLES

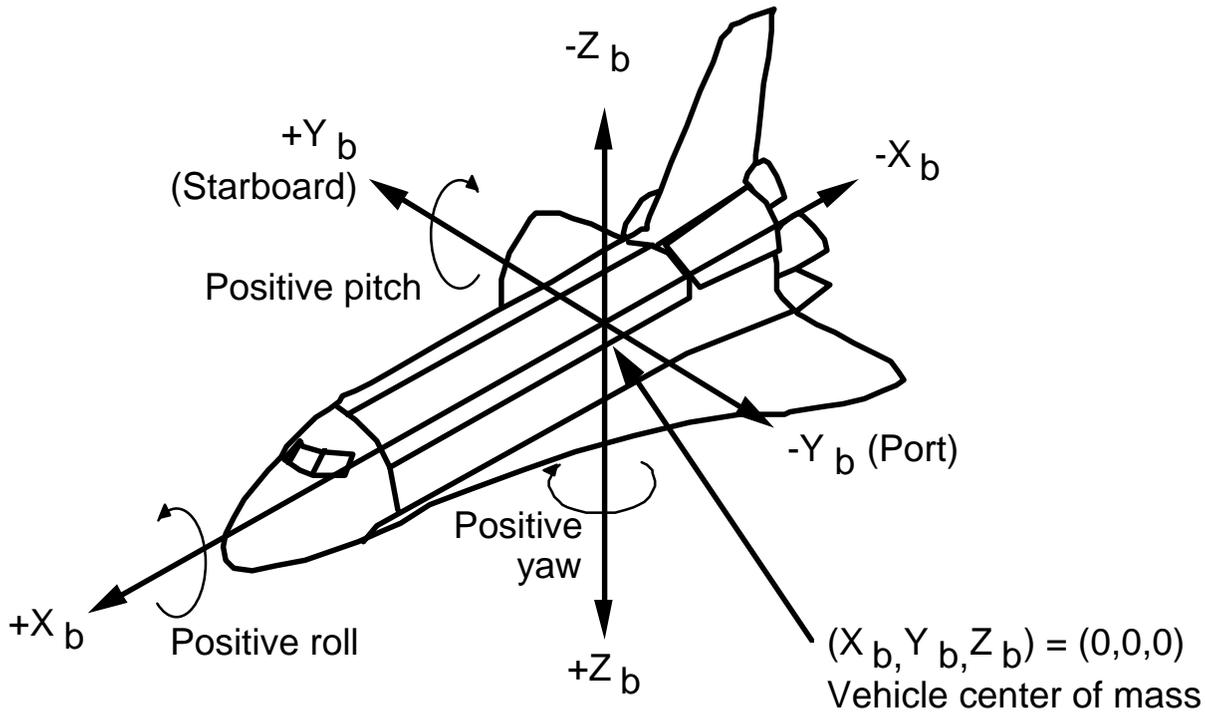
Figure 102: LMS, Head C (fc=25 Hz)



COORDINATE SYSTEMS

ORBITER

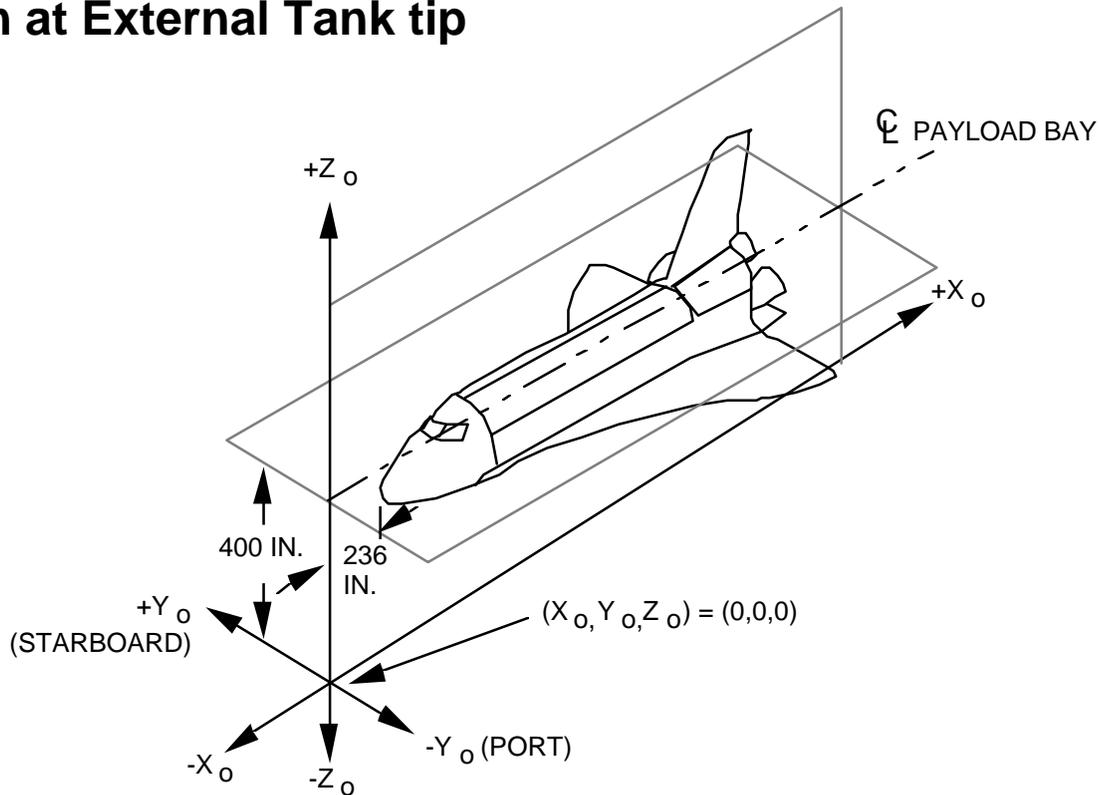
- **Body coordinate system**
 - origin at vehicle center of mass



COORDINATE SYSTEMS

ORBITER

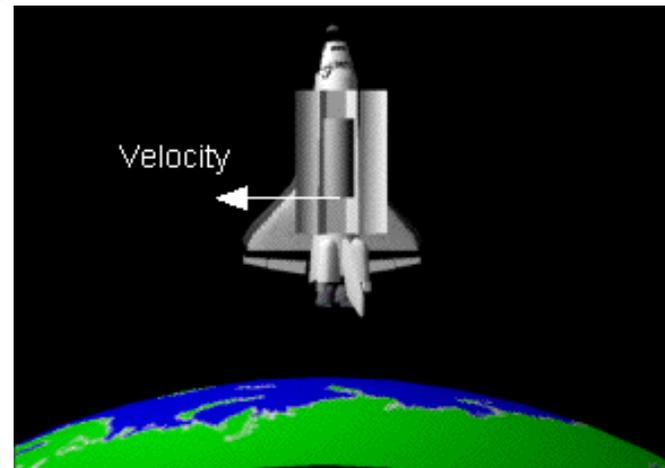
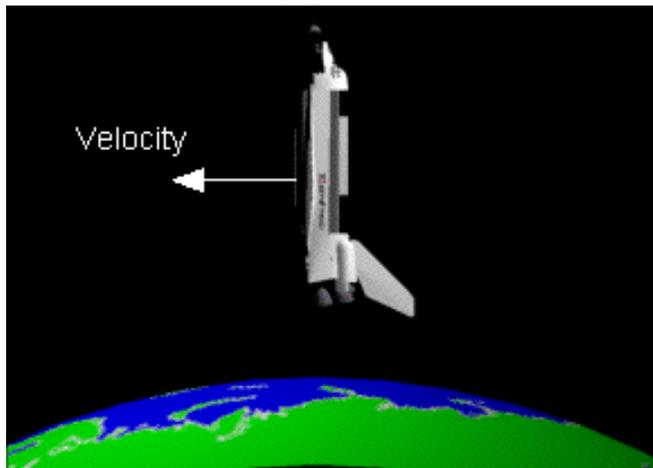
- **Structural coordinate system**
 - **origin at External Tank tip**



FLIGHT ATTITUDES

ORBITER

- Orbiter has two main attitudes
 - Local vertical / local horizontal (Earth oriented)
 - Inertial (quite often sun oriented)

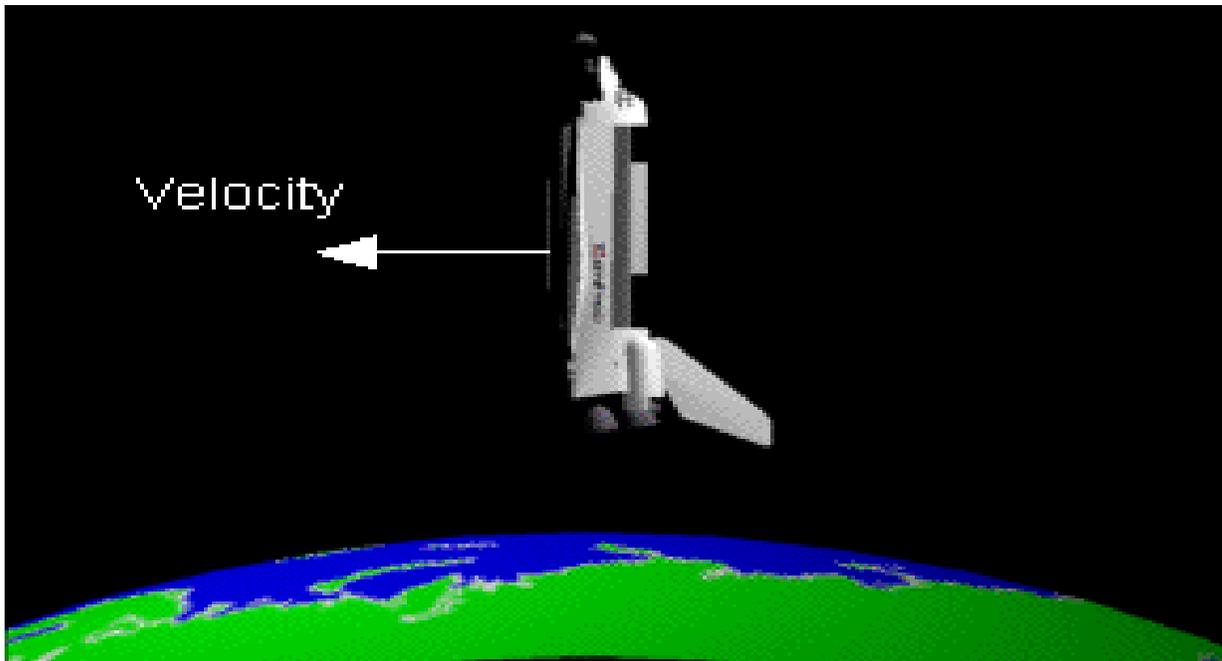


- Designation of attitudes
 - pitch / yaw / roll angle relative to airplane mode
 - e.g. PYR: 90°, 0°, 90°
 - body axes oriented to nadir (toward Earth) and flight direction
 - e.g. -XLV / +YVV

REFERENCE FRAME

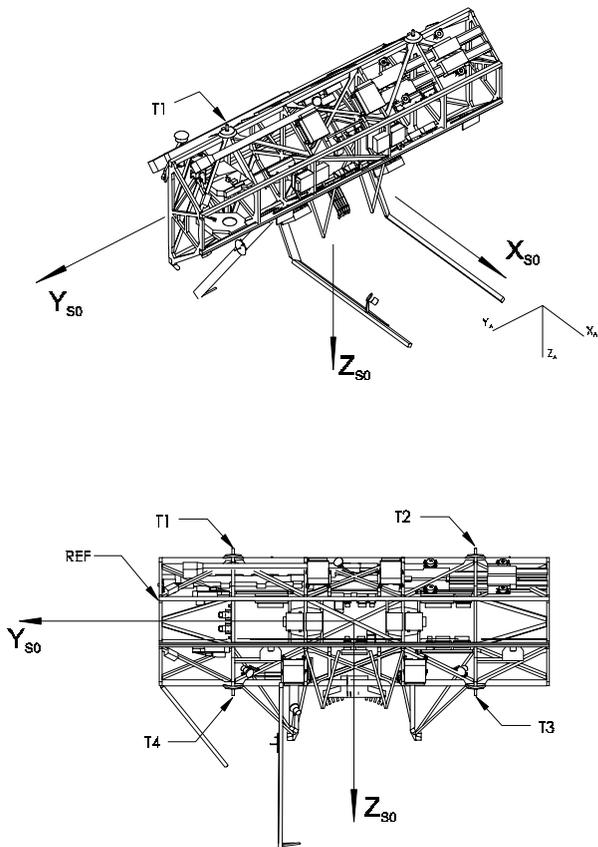
ORBITER

- **Fixed frame of reference determines sense of observed acceleration**
 - **Inertial reference frame: frame fixed with respect to inertial space**
 - **Science reference frame: frame fixed with respect to vehicle**

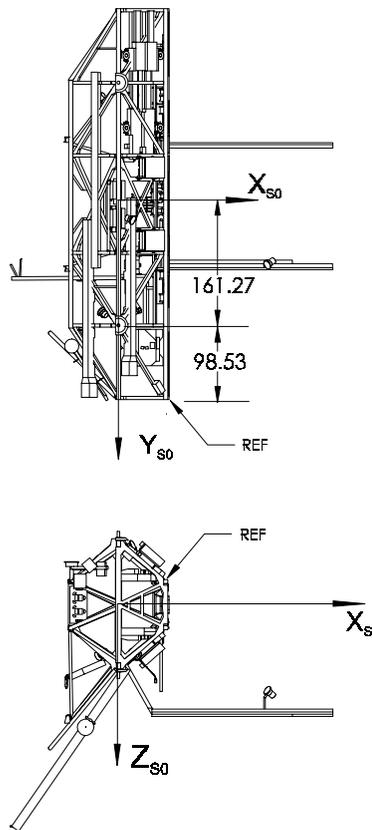


COORDINATE SYSTEMS

ISS



Integrated Truss Segment S0 Coordinate System



Type

Right-Handed Cartesian, Body-Fixed

Description

This coordinate system defines the origin, orientation, and sense of the Space Station Analysis Coordinate System.

Origin

The YZ plane nominally contains the centerline of all four trunnion pins. The origin is defined as the intersection of two diagonal lines connecting the centers of the bases of opposite trunnion pins, running T1 to T3 and from T2 to T4.

Orientation

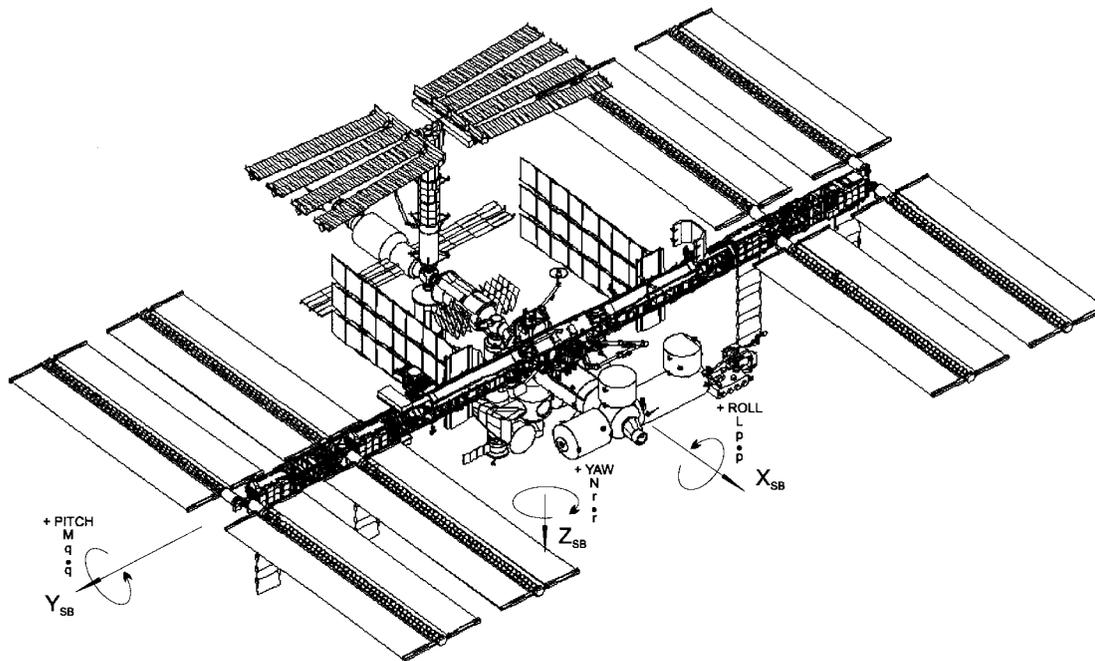
X_{S0}: The X-axis is parallel to the vector cross-product of the Y-axis with the line from the center of the base trunnion pin T2 to the center of the base trunnion pin T3, and is positive forward

Y_{S0}: The Y-axis is parallel with the line from the center of the base of trunnion pin T2 to the center of the base of trunnion pin T1. The positive Y-axis is toward starboard.

Z_{S0}: The Z-axis completes the RHCS

COORDINATE SYSTEMS

ISS



SPACE STATION ANALYSIS COORDINATE SYSTEM

Type

Right-Handed Cartesian, Body-Fixed

Description

This coordinate system is derived using the Local Vertical Local Horizontal (LVLH) flight orientation. When defining the relationship between this coordinate system and another, the Euler angle sequence to be used is a yaw, pitch, roll sequence around the Z_A , Y_A , and X_A axes, respectively.

Origin

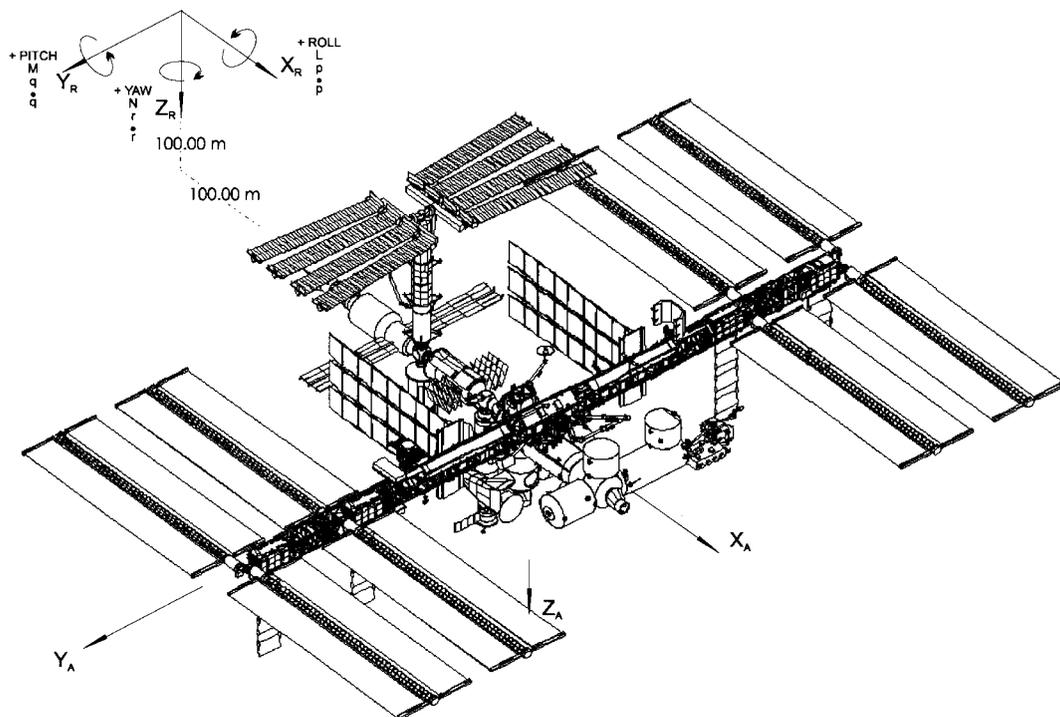
The origin is located at the geometric center of Integrated Truss Segment (ITS) S_0 and is coincident with the S_0 Coordinate frame.

Orientation

- X_A :** The X-axis is parallel to the longitudinal axis of the module cluster. The positive X-axis is in the the forward direction
- Y_A :** The Y-axis is identical with the S_0 axis. The nominal alpha joint rotational axis is parallel with Y_A . The positive Y-axis is in the starboard direction.
- Z_A :** The positive Z-axis is in the direction of nadir and completes the right-handed Cartesian system (RHCS).

COORDINATE SYSTEMS

ISS



SPACE STATION REFERENCE COORDINATE SYSTEM

Type

Right-Handed Cartesian, Body-Fixed

Description

This coordinate system is derived using the Local Vertical Local Horizontal (LVLH) flight orientation.

Origin

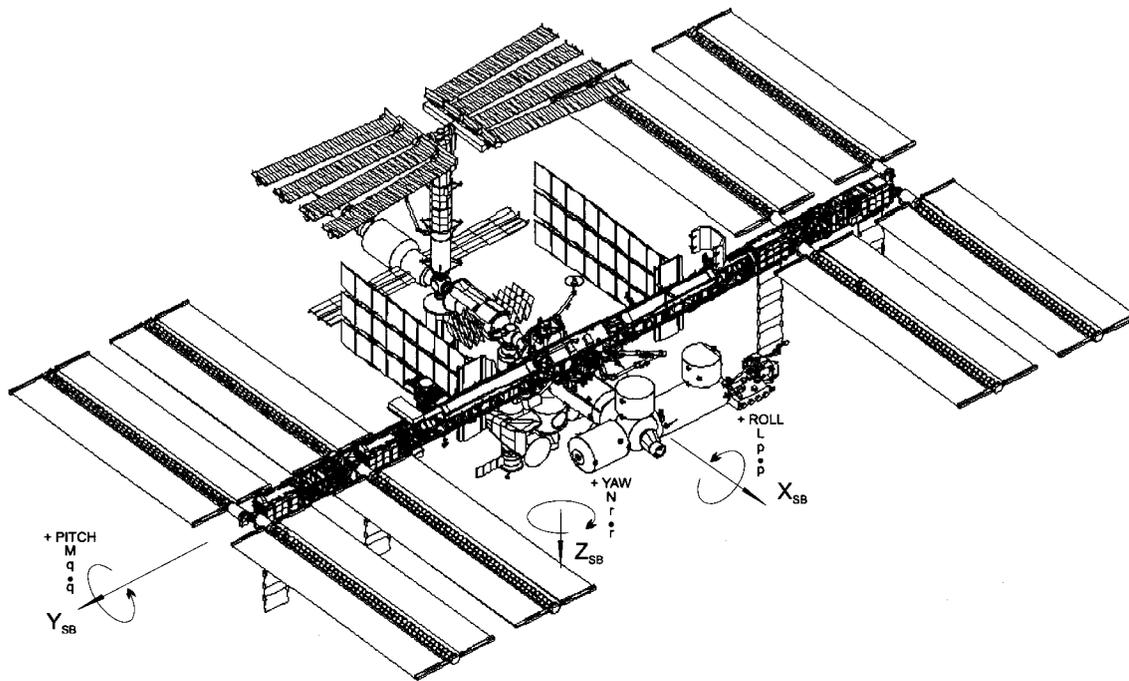
The datum point is located at the origin of the Space Station Analysis Coordinate System frame. The origin of the Space Station Reference Coordinate System is located such that the datum point is located at: $X_R=100$, $Y_R=0$, and $Z_R=100$ meters

Orientation

- X_R : The X-axis is parallel to the X_A . The positive X-axis is in the forward direction
- Y_R : The Y-axis is coincident with the nominal alpha joint rotational axis, which is parallel to Y_A . The positive Y-axis is in the starboard direction.
- Z_R : The positive Z-axis is parallel to Z_A and is in the direction of nadir and completes the rotating right-handed Cartesian system.

COORDINATE SYSTEMS

ISS



SPACE STATION BODY COORDINATE SYSTEM

Type

Right-Handed Cartesian, Body-Fixed

Description

When defining the relationship between this coordinate system and another, the Euler angle sequence to be used is a yaw, pitch, roll sequence around the Z_{SB} , Y_{SB} , and X_{SB} axes, respectively

Origin

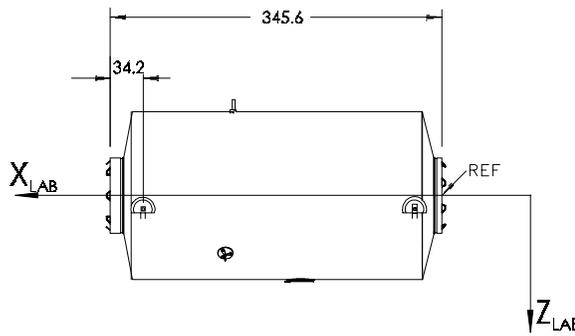
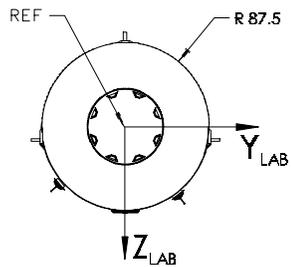
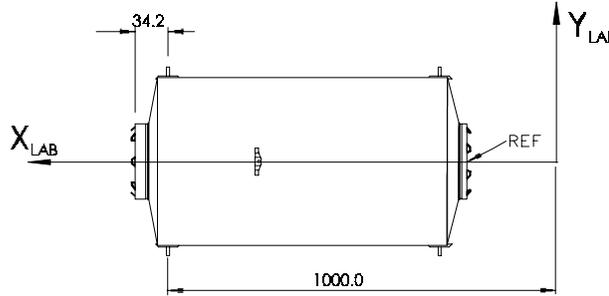
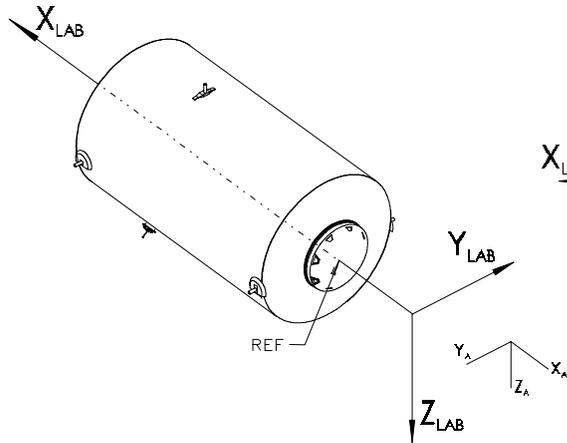
The origin is located at the Space Station center of mass.

Orientation

- X_{SB} :** This axis is parallel to the X_A axis. Positive X_{SB} is in the forward flight direction.
- Y_{SB} :** This axis is parallel to the Y_A . Positive Y_{SB} is toward starboard.
- Z_{SB} :** This axis is parallel with the Z_A . Positive Z_{SB} is approximately toward nadir and completes the right-handed system: X_{SB} , Y_{SB} , Z_{SB} .

COORDINATE SYSTEMS

ISS



Type

Right-Handed Cartesian, Body-Fixed to the Pressurized Module

Origin

The origin is located forward of the pressurized module such that the center of the bases of the aft trunnions have X_{LAB} components nominally equal to 1000.000 inches.

Orientation

X_{LAB} : The X-axis is perpendicular to the nominal aft CBM interface plane and pierces the geometric center of the array of mating bolts at the aft end of the pressurized module. The positive X-axis is toward the pressurized module from the origin.

Y_{LAB} : The Y-axis completes the right-handed Cartesian system (RHCS).

Z_{LAB} : The Z-axis is parallel to the perpendicular line from the X-axis to the center of base of the keel pin, and positive in the opposite direction as shown.

UNITED STATES LABORATORY MODULE COORDINATE SYSTEM

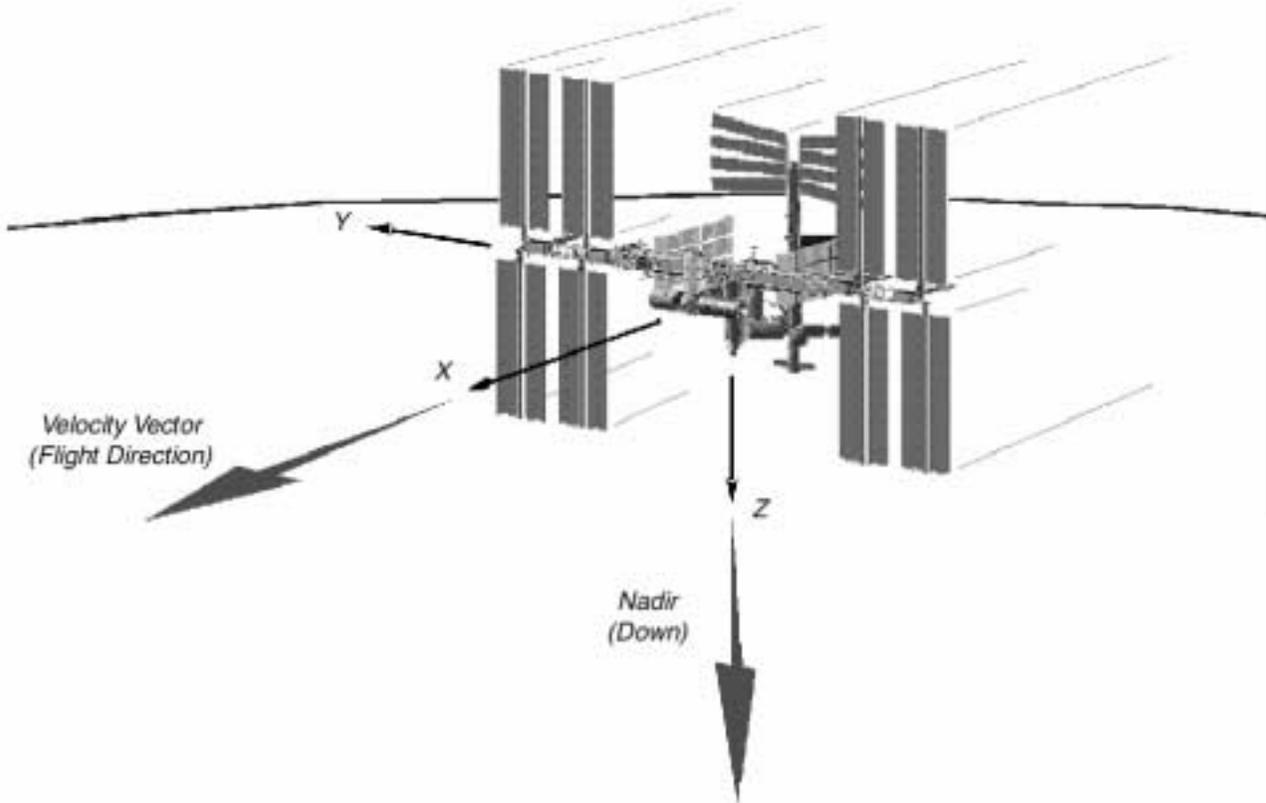
FLIGHT ATTITUDES

ISS

XVV Z Nadir: X Axis Near Velocity Vector, Z Axis Nadir/Down

XVV Z Nadir Flight Attitude Shown With 0, 0, 0 Deg. Yaw, Pitch, Roll LVLH Attitude

XVV TEA is Nearest Torque Equilibrium Attitude (TEA) To This Orientation



The basic flight attitude for ISS is called **XVV Z Nadir**. The vehicle design is optimized for this attitude. The **XVV** attitude:

- places the most modules in the microgravity volume
- supports altitude reboosts
- service vehicle dockings
- minimizes aerodynamic drag

The ISS is designed to tolerate deviations from perfect XVV Z Nadir of +/- 15 degrees in each axis. This envelope was expanded to -20 deg in pitch.



EXPERIMENT PLANNING AND EXECUTION

Available Reduced Gravity Carriers / Facilities

- **STS Orbiters**
- **International Space Station (ISS)**
- **Sounding Rockets**
- **Parabolic Flight Aircraft (KC-135)**
- **Free-Flyers**
- **Drop Towers**
- **Microgravity Emission Lab (MEL)**



EXPERIMENT PLANNING AND EXECUTION

Experiment Location and Orientation

- **Proximity to carrier / vehicle center of mass**
 - sensitivity to quasi-steady variations
- **Proximity to other equipment**
 - sensitivity to vibration sources
- **Alignment**
 - sensitivity to quasi-steady acceleration direction



EXPERIMENT PLANNING AND EXECUTION

Carrier Attitude

- **Issues related to experiment location**
 - gravity gradient effects
- **Issues related to experiment orientation**
 - design attitude that points experiment in desired direction
- **Sensitivity to quasi-steady variations with time**
 - atmospheric drag effects
 - local vertical / local horizontal attitudes versus inertial attitude



EXPERIMENT PLANNING AND EXECUTION

Accelerometer Selection

- **Frequency Range**
 - cutoff frequency based on experiment sensitivity
 - sampling rate and filter characteristics specified by accelerometer system team to provide frequency selected by experimenter
- **Location and Alignment**
 - close to experiment sensitive location
 - mounting technique
 - away from sources which may disturb accelerometer and mask disturbances of interest
 - knowledge of sensor orientation relative to experiment axes



EXPERIMENT PLANNING AND EXECUTION

Mission / Experiment Timeline

If at all possible, schedule your experiment operations to avoid any activities which might negatively impact it. Keep the following points in mind:

- **Experiment sensitivity to acceleration sources**
 - quasi-steady, vibratory and transient
- **Crew exercise**
- **Crew activity**
- **Thruster activity**
- **Other experiment operations**
- **Venting**

EXPERIMENT SENSITIVITY ASSESSMENT

ISS Microgravity Requirements

Summary

Quasi-steady

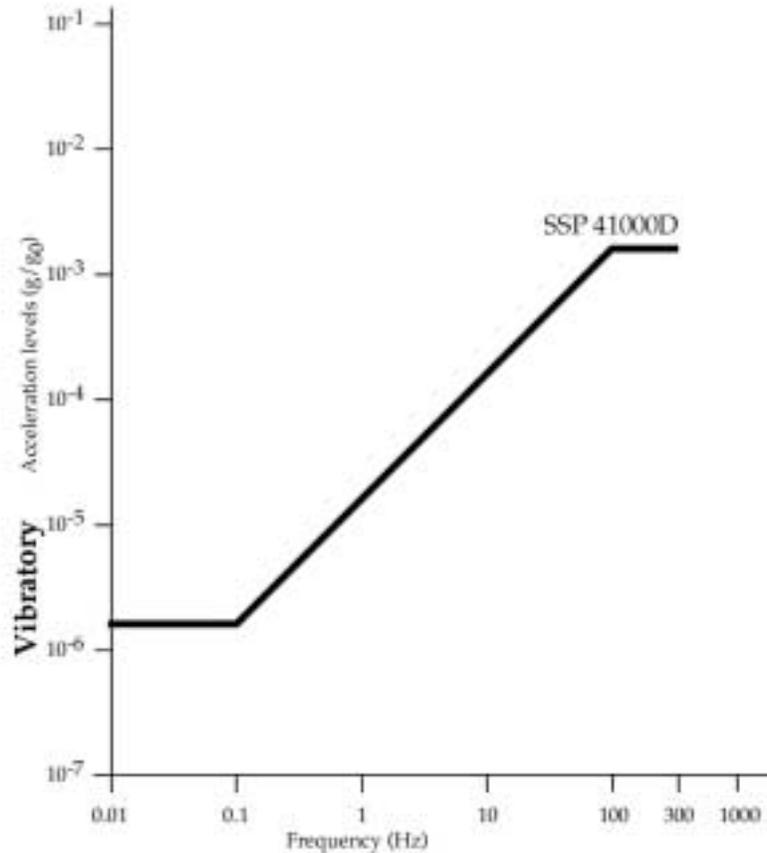
- Steady state $< f < 0.01$ Hz
- $g \leq 1 \mu g_{rms}$
- Stability: perpendicular $g \leq 0.2 \mu g_{rms}$

Vibratory

- Levels in figure at structural mounting interfaces
- RMS acceleration magnitude in one-third octave averaged over 100 seconds
- Does not include crew disturbances

Transient

- $g \leq 1000 \mu g$ per axis
- $g \leq 10 \mu g\text{-sec}$ per axis (integrated over 10 sec)



EXPERIMENT SENSITIVITY ASSESSMENT

ISS Microgravity Environment

THE Requirement for the International Space Station

DURATION

QUASI-STEADY

Mode: Microgravity - habitable
 This mode consists of capabilities required for microgravity research by user payloads in a habitable environment. This mode does not include the effects of crew activity, but does include the effects of crew equipment, such as the operation of exercise devices and latched or hinged enclosures. Crew effects will be mitigated to the extent possible. This mode consists of the capabilities described in SSP 41000 and the following unique capability.

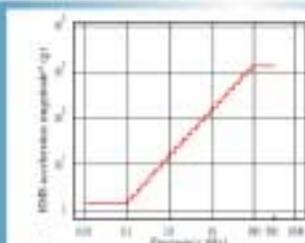
Capability: Support microgravity experiments
 The purpose of this capability is to establish the required environment for microgravity experiments. The Space Station shall provide the following microgravity acceleration performance for at least 50 percent of the internal payload locations (excluding Nadir window payload location) for 180 days per year in continuous time intervals of at least 30 days:

VIBRATORY

TRANSIENT

- a. At the centers of the internal payload locations, a quasi-steady (<math>f < 0.01 \text{ Hz}</math>) acceleration
 - (1) Magnitude less than or equal to 1 micro-g
 - (2) Component perpendicular to the orbital average acceleration vector less than or equal to 0.2 micro-g
- b. At the structural mounting interfaces to the internal payload locations
 - (1) A vibratory acceleration limit as defined in the figure below.
 - (2) A transient acceleration limit for individual transient disturbance sources less than or equal to 1000 micro-g per axis
 - (3) An integrated transient acceleration limit for individual transient disturbance sources less than or equal to 10 micro-g seconds per axis over any 10 second interval

The Space Station shall monitor and record the microgravity environment at selected locations.



For $0.01 < f < 0.1 \text{ Hz}$ $a \leq 1.0 \mu\text{g}$
 For $0.1 < f < 10 \text{ Hz}$ $a \leq f \times 10 \mu\text{g}$
 For $10 < f < 100 \text{ Hz}$ $a \leq 1000 \mu\text{g}$
 where: f = frequency
 a = acceleration

*NOTE: Root-mean-square acceleration magnitude is 1.5 times peak average over 100 seconds.

Vibratory microgravity acceleration limits for the International Space Station reflect:

EXPERIMENT SENSITIVITY ASSESSMENT

Fundamental Physics

Quasi-steady

- A large quasi-steady level will destroy sample uniformity of critical fluid

Vibratory

- Primary concern is vibratory heating of sample and destruction of sample uniformity

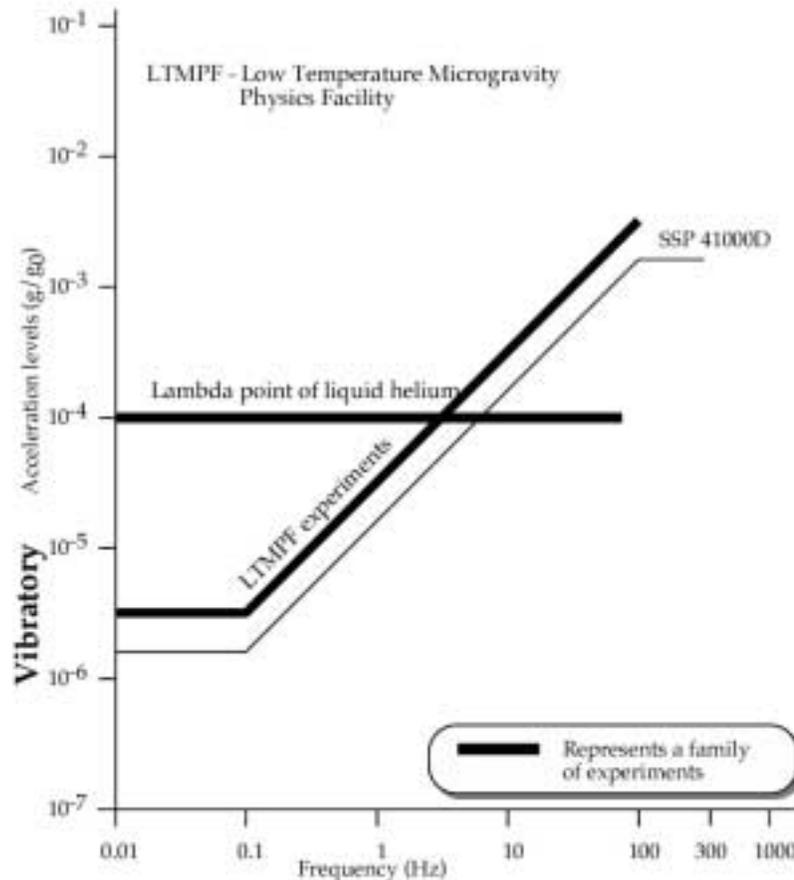
Transient

- Primary concern is vibratory heating of sample and destruction of sample uniformity

Rationale

- Low temperature physics experiments rely on establishment of highly uniform sample in microgravity

-
- NOTE: Many of these experiments are expected to be operated on the JEM-EF



EXPERIMENT SENSITIVITY ASSESSMENT

Combustion Science

Quasi-steady

- Not a major concern ($10^{-4} g_0$)

Vibratory

- Typically low acceleration levels at low frequencies (< 1 Hz) disturb experiments
- Most experiments are above the ISS requirement curve but some are below the expected environment
- Low frequency g-jitter has been observed repeatedly to affect the combustion characteristics of a variety of flames, e.g., candle, gas jet, flame balls, etc.

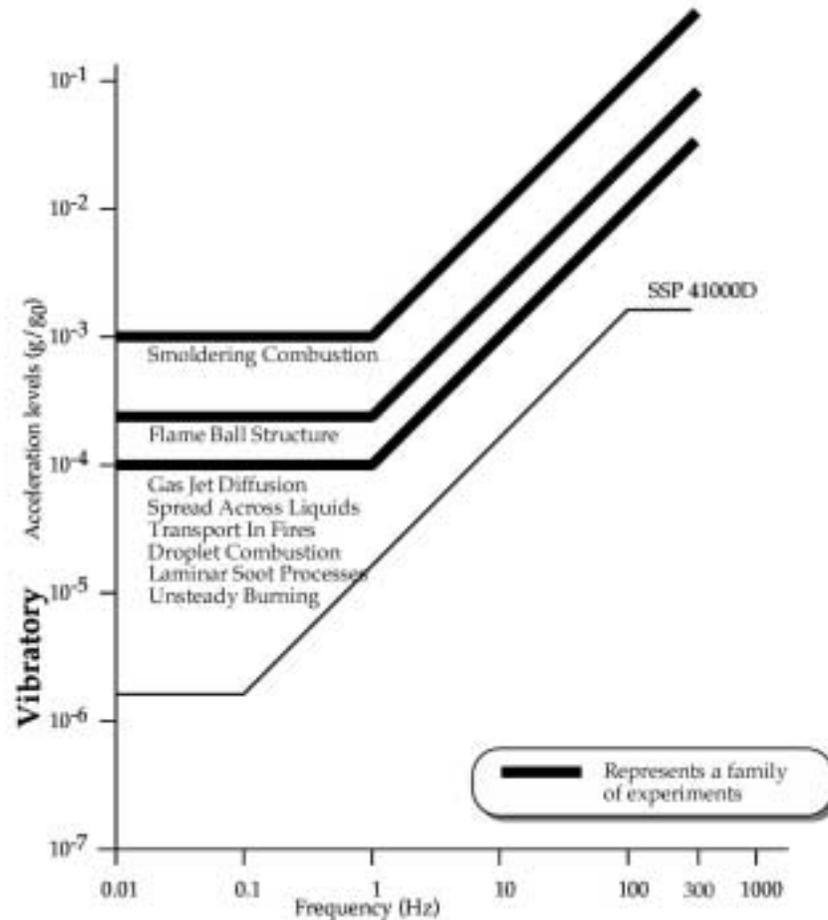
ref: Dr. H. Ross / NASA LeRC

Transient

- Tolerable for most experiments with time and magnitude restrictions on the disturbance

Rationale

- Microgravity conditions allow:
 - isolation of gravity-driven mechanisms;
 - influence of transport phenomena
 - creation of symmetry and / or boundary & initial conditions
 - new diagnostic probing or testing of similitude
- Microgravity environment has attracted widespread external peer advocacy for combustion science in space



EXPERIMENT SENSITIVITY ASSESSMENT

Biotechnology

Quasi-steady

- Not a major concern (10^{-3} to 10^{-4} g_0)

Vibratory

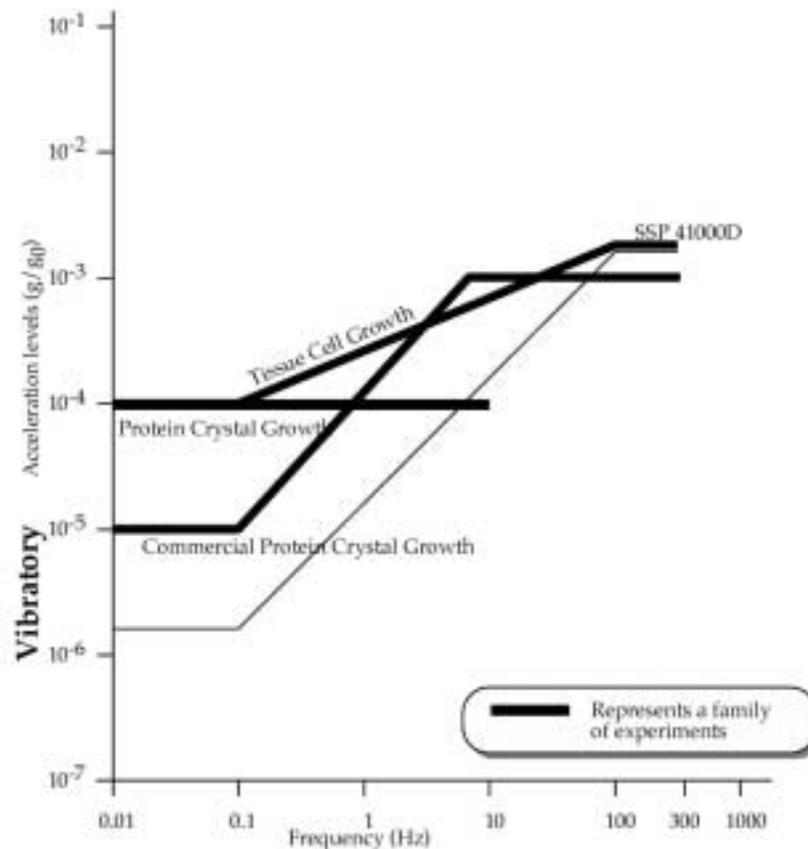
- Impact at higher frequencies of the desired operating level

Transient

- Primary concern is for large scale accelerations, such as Orbital Maneuvering System engines and crew disturbances

Rationale

- Large disturbances cause nucleations to occur in multiple sites destroying single crystal formation



EXPERIMENT SENSITIVITY ASSESSMENT

Fluid Physics

Quasi-steady

- Quasi-steady accelerations disturb most fluid experiments ($2 \times 10^{-6} g_0$)

Vibratory

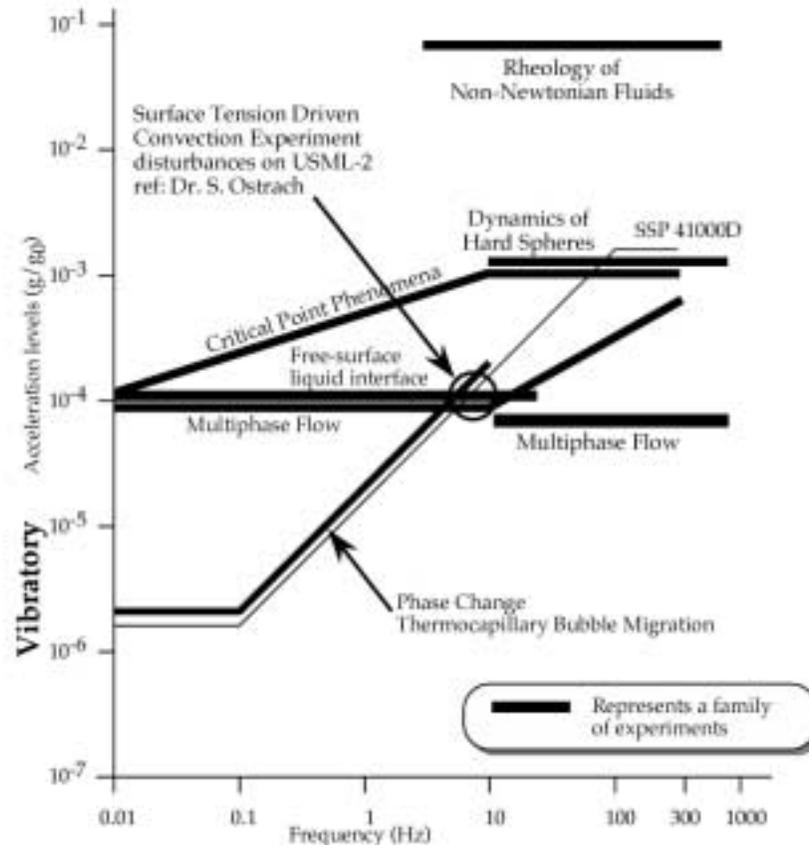
- Mid-range frequencies of expected environment will disturb fluid free surface experiments
- Some experiments require environment at lower levels than the ISS requirements curve e.g. Thin Film Fluid Flows at Menisci
- Surface Tension Driven Convection Experiment experienced surface distortion due to g-jitter frequently throughout the USML-2 mission
ref: Dr. S. Ostrach/CWRU

Transient

- Transients disturb fluid experiments with lower viscosity fluids

Rationale

- Accelerations above a threshold cause interface instability, density settling, and density-driven convection & mixing



EXPERIMENT SENSITIVITY ASSESSMENT

Materials Science

Quasi-steady

- Some samples and processes require very low quasi-steady acceleration levels ($a < 0.1$ micro-g)
e.g., Stoke's settling, Bridgman growth, Float zone
- Residual acceleration direction and stability are important factors for crystallization processes
- A Crystal Growth Furnace sample was withdrawn from USML-2 due to a change in Orbiter attitude just before launch
ref: Dr. S. Lehoczyk/NASA MSFC

Vibratory

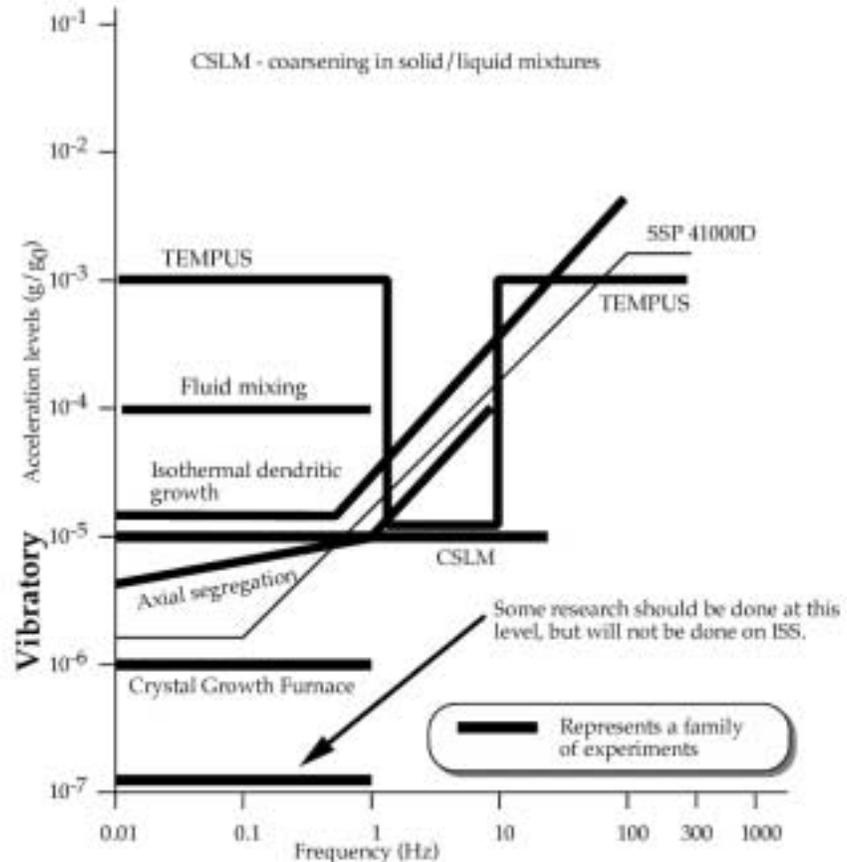
- Disturbances in various frequency ranges disturb experiments involving molten samples, suspended samples, etc.

Transient

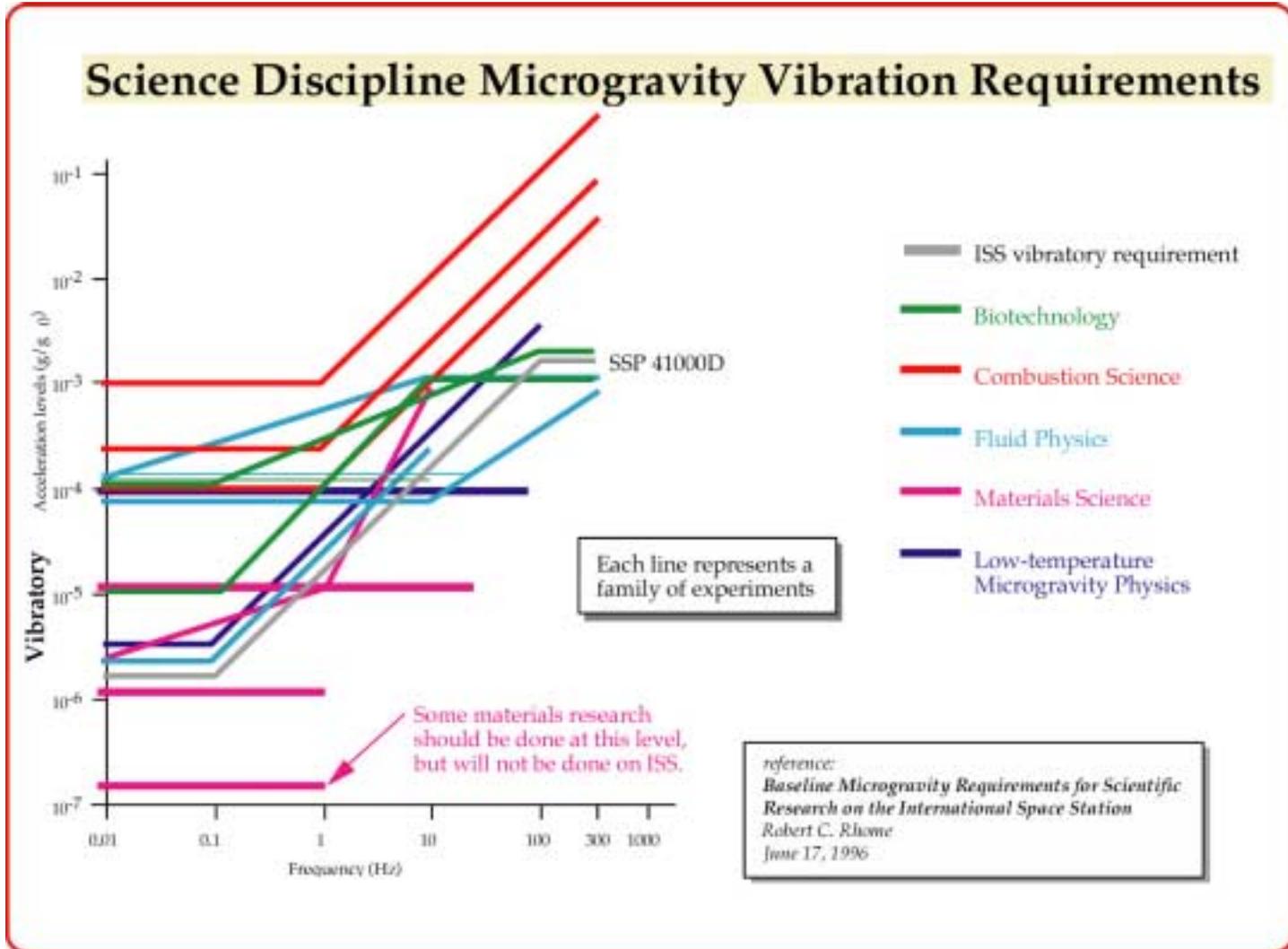
- Some processes are very susceptible to transients such as thruster firings
- MEPHISTO (USMP-1 & USMP-3) experienced effects which lasted minutes from single thruster firings (0.01 g for 10 - 25 seconds)

Rationale

- Accelerations above a threshold cause thermo-solutal convection and interface instability



EXPERIMENT SENSITIVITY ASSESSMENT





EXPERIMENT SENSITIVITY ASSESSMENT

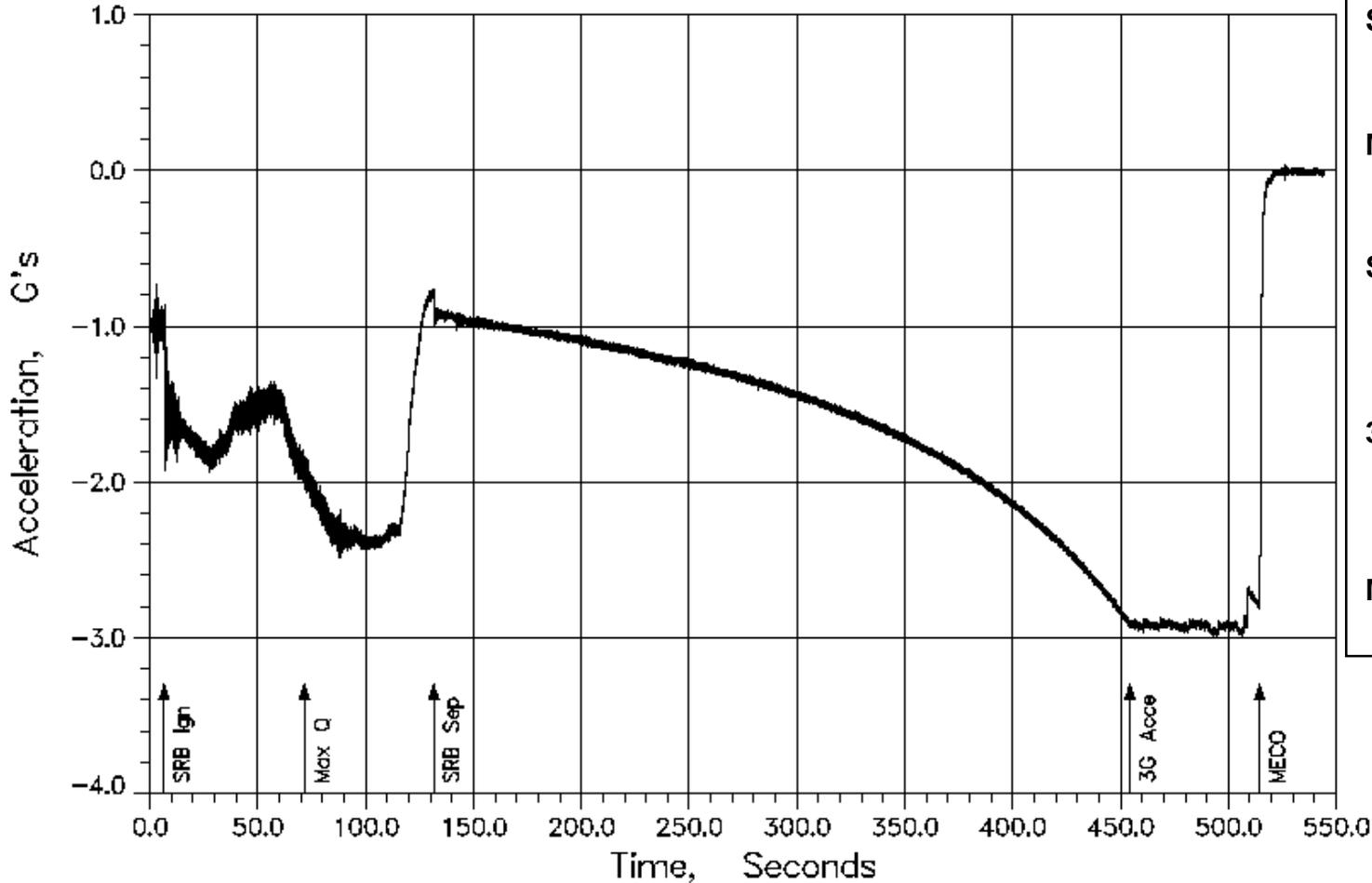
Experiment Type	Frequency Range	Measurement Level
Biotechnology	QS – 10 Hz	100 μg and above
Fluid Physics	QS – 300 Hz	1 μg to 1 mg
Combustion Science	QS – 50 Hz	10 μg and above
Fundamental Physics	QS – 180 Hz	0.1 μg and above
Material Science	QS – 300 Hz	0.01 μg and above

STS ASCENT PROFILE

STS-90 Payload Bay Ascent Data - SSME Ing=0.0 second (0-50 Hz)

V34A9483A, DOF: X, Location: x=1029.0, y=-101.0, z=408.0

SRB-Ign=6.56, Max-Q=71.57, SRB-Sep=131.57, 3G-Acce=454.37, MECO=514.57



STS = Columbia

SRB_{ign} = solid rocket boosters ignition

Max Q = time of maximum dynamic pressure

SRB_{Sep} = solid rocket boosters separation

3G Acce = time at which 3g acceleration is reached

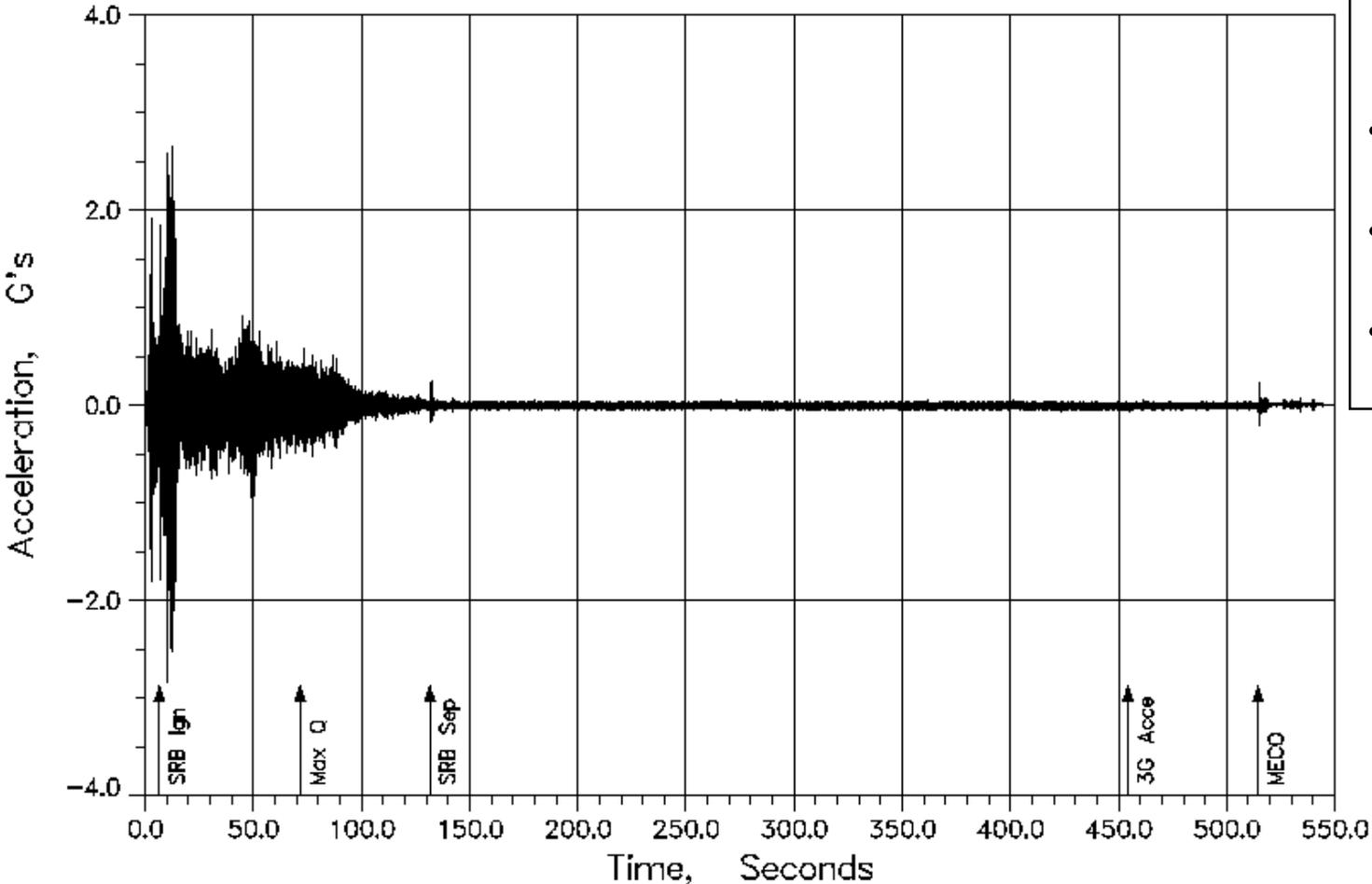
MECO = main engine cutoff

STS ASCENT PROFILE

STS-90 Payload Bay Ascent Data - SSME Ign=0.0 second (0-50 Hz)

V34A9460A, DOF: Y, Location: x=701.0, y=-102.0, z=407.0

SRB-Ign=6.56, Max-Q=71.57, SRB-Sep=131.57, 3G-Acce=454.37, MECO=514.57



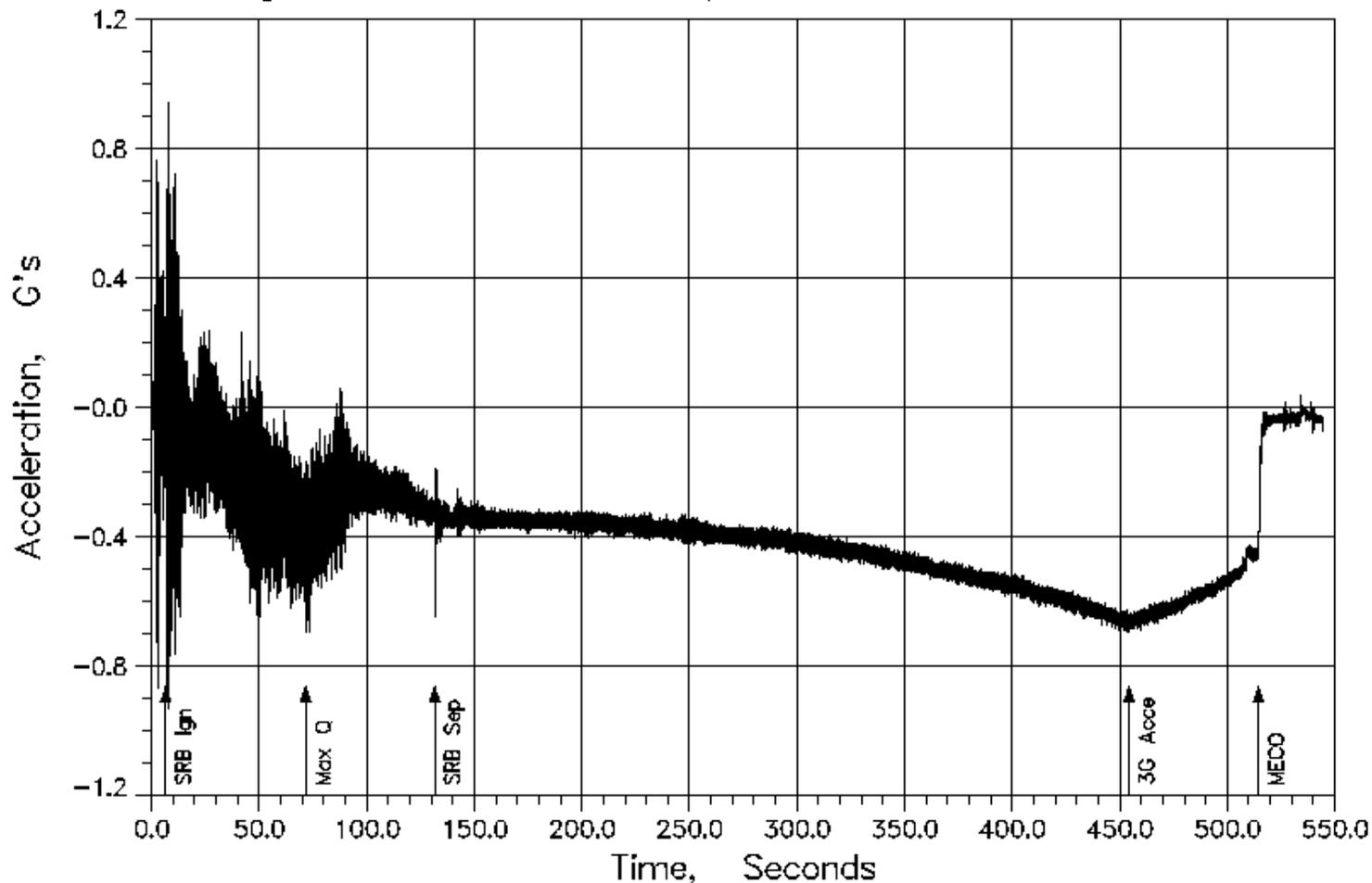
- **Sensor dynamic responses:**
-10 to + 10 G range
- **Frequency response:**
0 – 50 Hz
- **Sampling rate:**
500 samples per sec.
- **Coordinate system:**
Orbiter structural system

STS ASCENT PROFILE

STS-90 Payload Bay Ascent Data - SSME Ign=0.0 second (0-50 Hz)

V34A9461A, DOF: Z, Location: x=701.0, y=-102.0, z=407.0

SRB-Ign=6.56, Max-Q=71.57, SRB-Sep=131.57, 3G-Acce=454.37, MECO=514.57

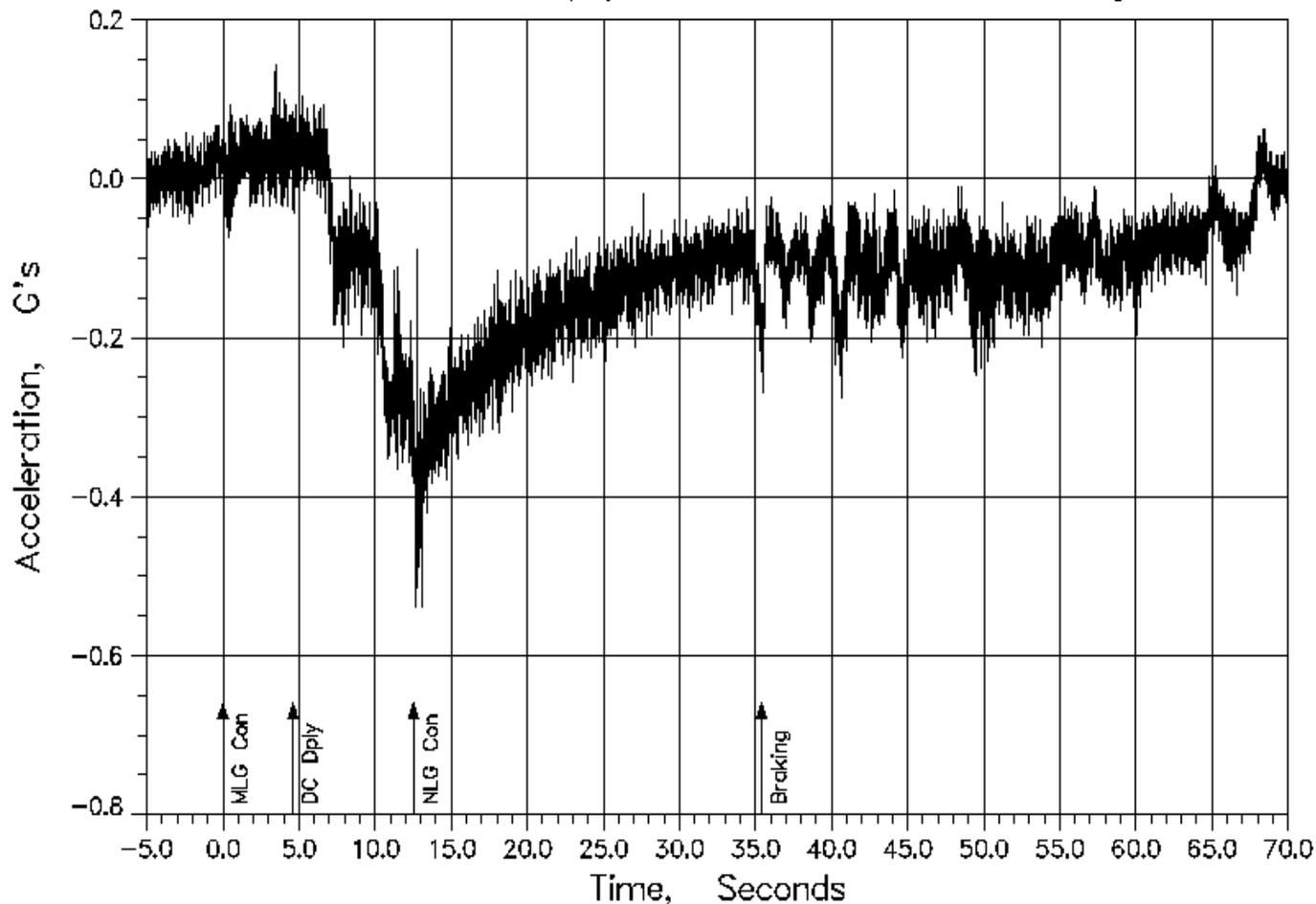


STS LANDING PROFILE

STS-92 Payload Bay Landing Time History

V34A9469A, DOF: X, Location: x=878.0, y=-102.0, z=407.0

MLG Contact=0.00s, DC Deploy=4.60s, NLG Contact=12.52s, Braking=35.40s



STS = Discovery

MLG_{cont} = main landing gear ground contact

DC_{deploy} = drag Chute deployment

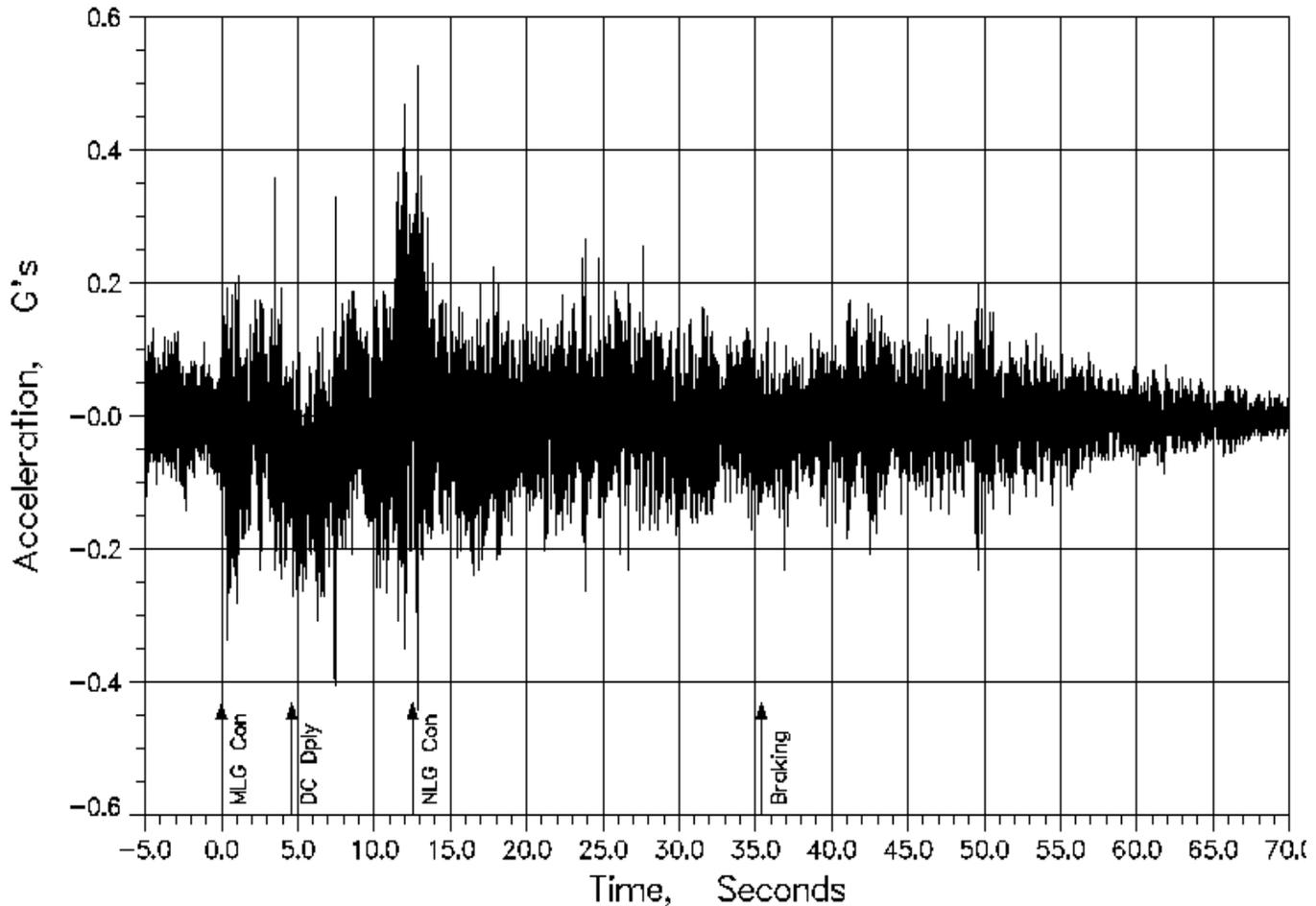
NLG_{cont} = noise landing gear ground contact

STS LANDING PROFILE

STS-92 Payload Bay Landing Time History

V34A9460A, DOF: Y, Location: x=701.0, y=-102.0, z=407.0

MLG Contact=0.00s, DC Deploy=4.60s, NLG Contact=12.52s, Braking=35.40s

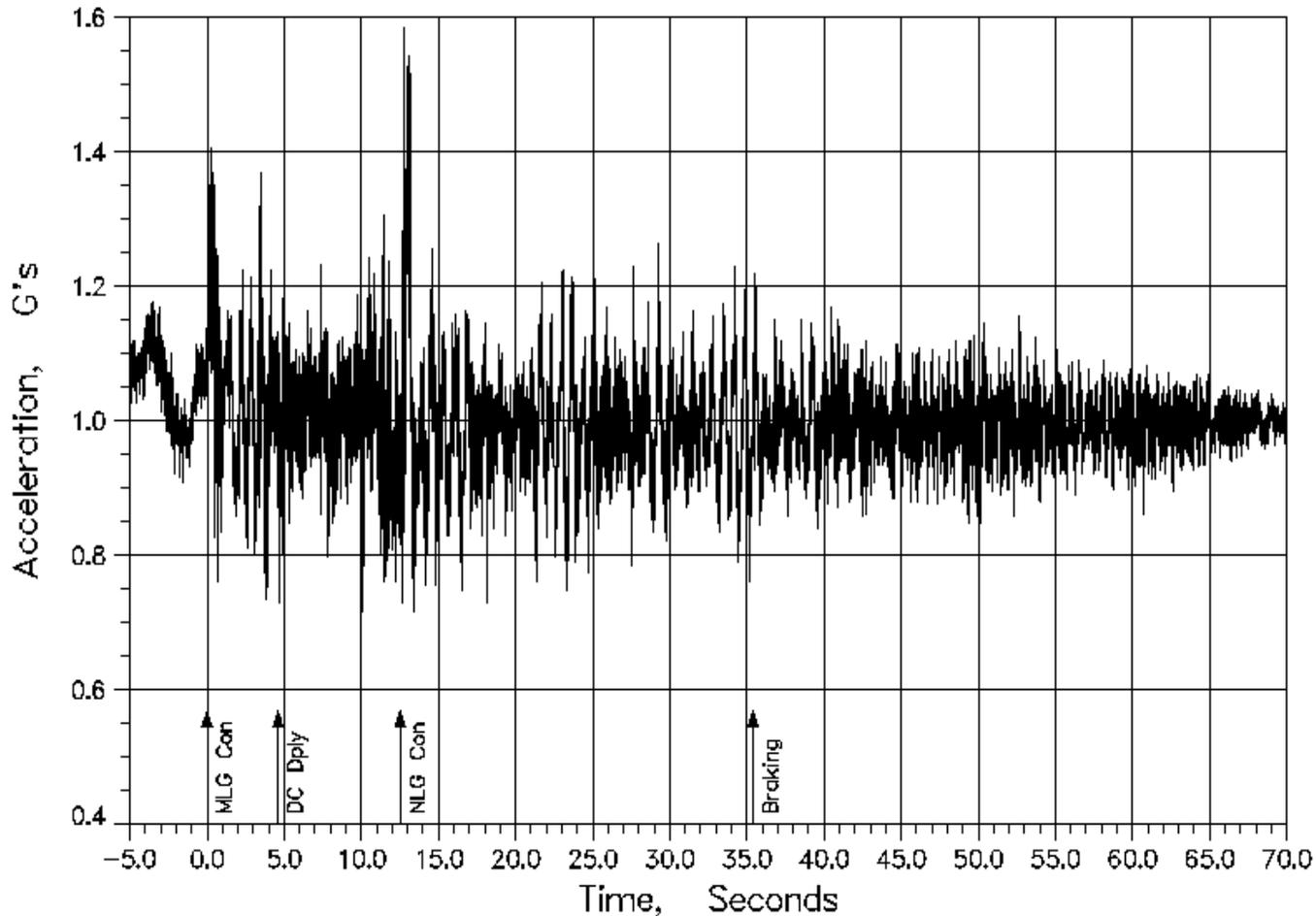


STS LANDING PROFILE

STS-92 Payload Bay Landing Time History

V34A9461A, DOF: Z, Location: x=701.0, y=-102.0, z=407.0

MLG Contact=0.00s, DC Deploy=4.60s, NLG Contact=12.52s, Braking=35.40s

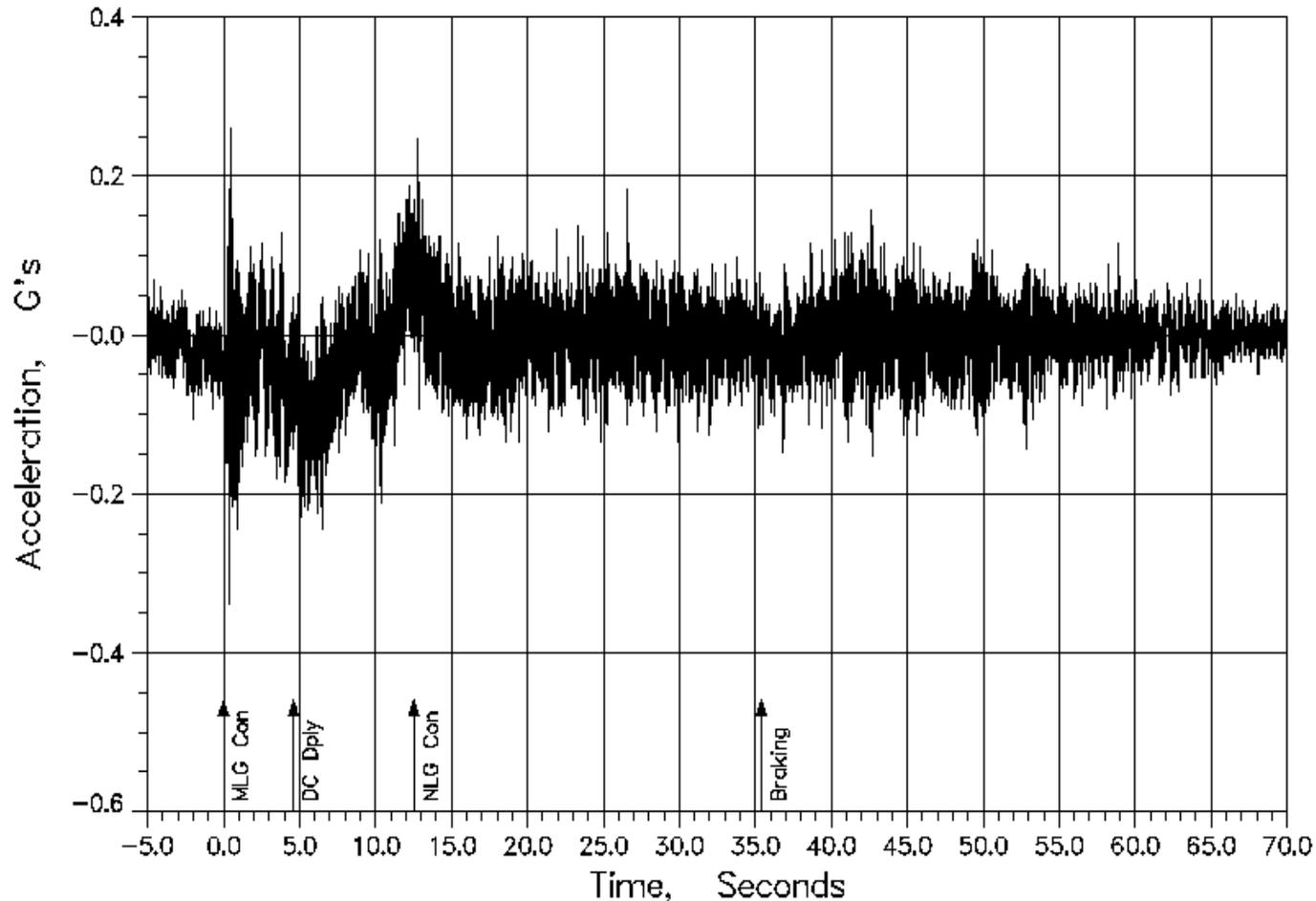


STS LANDING PROFILE

STS-92 Payload Bay Landing Time History

V34A9480A, DOF: Y, Location: x=919.0, y=-7.0, z=305.0

MLG Contact=0.00s, DC Deploy=4.60s, NLG Contact=12.52s, Braking=35.40s





OVERALL SUMMARY

- **The reduced gravity environment is not “zero-g” or even “zero-acceleration”. It is dynamic.**
- **The environment may (and will) influence the results of a science experiment.**
- **Analyses and/or tests should be performed before flight to investigate the sensitivity of an experiment to the reduced gravity environment.**
- **Environments of past missions should be considered in planning future experiments.**
- **Experiment teams should be concerned about what disturbances they may be causing to the environment with (for example) moving parts from their experiments or / and required crew actions.**



REFERENCES

- DeLombard, R.: “Compendium of Information for Interpreting the Microgravity Environment of the Orbiter Spacecraft.” NASA TM-107032, 1996.
- Rogers, M. J. B., Hrovat, K., McPherson, K., Moskowitz, M. E., and Reckart, T.: Accelerometer Data Analysis and Presentation Techniques, NASA TM-113173, September 1997.
- DeLombard, R.; McPherson, K.; Hrovat, K; Moskowitz, M.; Rogers, M. J. B.; and Reckart, T.: Microgravity Environment Description Handbook, NASA TM-107486, 1997.
- Sutliff, T. J.: Requirements and Development of an Acceleration Measurement System for International Space Station Microgravity Science Payloads, NASA TM-107484, June 1997.
- “International Space Station Flight Attitudes” D-684-10198-06 DCN-002, Dec. 1999.
- Robert C. Rhome.: “Baseline Microgravity Requirements for Scientific Research on the International Space Station”, June 1996.
- “System Specification for the International Space Station”, SSP 41000E, July 1996.
- Melissa J. B. Rogers.: “ Planning Experiments for a Microgravity Environment”, Sept. 1998.
- “Space Station Reference Coordinate Systems”, SSP 30219, Revision E, Nov. 1998.
- “Microgravity Control Plan”, SSP 50036RB, March 2000.
- Bao, Nguyen.: “STS-92 Payload Bay Flight and Analytical Ascent Data Assessment” MSAD-01-0140, Jan. 2001, Lockheed Martin Space Operation